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Active faulting and heterogeneous deformation across a megathrust segment boundary from GPS data, south-central Chile (36-39° S)

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Abstract.

This study focuses on the present-day deformation mechanisms of the south-central Chile margin, at the transition zone between two megathrust-earthquake segments defined from historical data: the Valdivia and Concepción sectors. New GPS data and finite-element models with complex geometries constrained by geophysical data are presented to gain insight into forearc kinematics and to address the role of upper-plate faults on contemporary deformation. GPS vectors are heterogeneously distributed in two domains that follow these two earthquake segments. We find that models which simulate only interseismic locking on the plate interface fail to reproduce surface deformation in the entire study area. In the Concepción domain, models that include a crustal-scale fault in the upper plate better reproduce the GPS observations. In the Valdivia domain, GPS data show regional-scale vertical-axis rotations, which could reflect postseismic deformation processes at the edge of the M_w 9.5 earthquake that ruptured in 1960 and/or activity of another crustal fault related to motion of a forearc sliver. Our study suggests that upper-plate faults in addition to earthquake-cycle transients may exert an important control on the surface velocity of subduction-zone forearcs.

1. Introduction

Contemporary deformation along active subduction margins primarily responds to the phases of the earthquake cycle [e.g., *Thatcher and Rundle, 1979; Thatcher, 1984*]. This cycle is a transient and repetitive process conditioned by the mechanical coupling between the continental and oceanic plates. During the interseismic phase of the earthquake cycle, high coupling between both plates results in the accumulation of contractional strain across the continental plate, as shown by numerical and analytical models constrained by geodetic data [e.g., *Savage et al., 1981; Hyndman and Wang, 1995; Mazzotti et al., 2000*]. The distribution of interseismic contractional strain is thought to be generally ruled by the width of the interplate seismogenic zone and its degree of locking [e.g., *Savage, 1983*]. The strain accumulated during the interseismic phase is mostly elastic and almost completely recovered by earthquake-related fault motion during the coseismic phase of the cycle [e.g., *Allmendinger et al., 2007*]. Coseismic earthquake rupture may be followed by a transient phase of postseismic deformation when either aseismic fault slip [e.g., *Tse and Rice, 1986; Hsu et al., 2006*] and/or prolonged viscoelastic relaxation of the mantle may occur [e.g., *Rundle, 1978*].

Although most of the forearc deformation is controlled by the megathrust, faults in the upper plate may contribute in releasing the elastic strain accumulated by plate convergence, either during an earthquake as documented in Alaska [*Plafker, 1972*] and postulated in Japan [*Park et al., 2002*], New Zealand [*Barnes et al., 2002*] and Chile [*Melnick et al., 2006a*], or presumably during the interseismic phase [e.g., *McCaffrey and Goldfinger, 1995; McCaffrey et al., 2007*], or both. The effect of motion on these upper-plate faults is ex-

pressed as short wavelength, but high-amplitude deformation localized in the vicinity of the structure. These faults may be crustal-scale features rooted in the subduction interface and long-lived, controlling the formation of forearc basins over millions of years [e.g., *Barnes et al.*, 2002; *Melnick et al.*, 2006a]. In some subduction zones where plate convergence is oblique to the margin, forearc slivers may develop, which can translate and rotate decoupled from the rest of the continent by forearc or intra-arc faults systems [e.g., *Fitch*, 1972; *Jarrard*, 1986; *Beck et al.*, 1993; *Wallace et al.*, 2004; *McCaffrey et al.*, 2007].

The south-central Chile margin has been the locus of several great subduction earthquakes in the past centuries, particularly the giant 1960 Valdivia event that reached moment magnitude (M_w) 9.5 (Figure 1a), the largest recorded instrumentally [*Kanamori*, 1977]. The region adjacent to the 1960 event ruptured last during the 1835 Concepción earthquake, which had an estimated magnitude of 8.5 [*Lomnitz*, 2004]. Several modeling studies constrained by GPS data have shown that the region of the 1960 earthquake is still in the postseismic phase whereas the region of the 1835 event is in the interseismic period [*Klotz et al.*, 2001; *Khazaradze et al.*, 2002; *Ruegg et al.*, 2002; *Hu et al.*, 2004]. Several active faults have been described in the Valdivia and Concepción regions [*Melnick and Echtler*, 2006], some of which are associated with clusters of crustal seismicity (Figure 1) [*Haberland et al.*, 2006; *Melnick et al.*, 2006a]. In this study, we focus on the overlapping segment boundary between the 1960 and 1835 earthquake rupture zones. We use GPS data and finite-element models with geometrical constraints given by various geophysical data to quantify the motion of upper plate faults and to address their role on the kinematics of the forearc. We find that numerical models that introduce faulting in the upper plate better reproduce the surface velocity field derived from GPS observations.

2. Seismotectonic Setting

The Chile margin is formed by oblique subduction of the Nazca oceanic plate under the South American continent at a present-day convergence rate of 66 mm/yr [Angermann *et al.*, 1999; Kendrick *et al.*, 2003]. Along the Chile margin, repeated historical earthquake ruptures have defined major seismotectonic segments [Lomnitz, 2004]. In south-central Chile, the adjacent Concepción and Valdivia segments have generated several large-magnitude events described in the \sim 500-year-long historical record [Lomnitz, 2004; Cisternas *et al.*, 2005]. The northern Concepción segment ($35\text{-}37.5^\circ$ S) (Figure 1a) ruptured last in 1835 [Darwin, 1839], with an earthquake of magnitude \sim 8.5 [Lomnitz, 2004]. The southern Valdivia 1960 segment ($37.5\text{-}46^\circ$ S), in turn, ruptured last during the great 1960 Chile earthquake. This event ruptured about 1000 km of the Nazca-South America plate boundary involving up to 40 m of fault slip resulting in up to 5.7 m of vertical coastal uplift [Plafker and Savage, 1970; Barrientos and Ward, 1990]. At present, these segments are thought to be in different phases of the seismic cycle [Barrientos *et al.*, 1992; Klotz *et al.*, 2001; Ruegg *et al.*, 2002]. The deformation pattern in the 1835 earthquake segment has been interpreted to represent strain accumulation due to locking of the megathrust during the interseismic phase [Ruegg *et al.*, 2002]. In turn, surface deformation in the 1960 earthquake segment has been thought to include the effects of protracted postseismic mantle rebound in addition to locking of the seismogenic zone [Khazaradze *et al.*, 2002; Hu *et al.*, 2004]. This interpretation arises from the fact that inland sites (along the intra- and back-arc zones) move in the opposite direction to coastal sites [Klotz *et al.*, 2001; Wang *et al.*, 2007].

The Arauco-Nahuelbuta forearc block is formed by the Arauco Peninsula, a major promontory along South America's Pacific coast and the Nahuelbuta Range, an abnormally-high segment of the Coastal Cordillera (Figure 1a). Here, active crustal faults have been mapped and described based on deformed coastal geomorphic features, seismic-reflection profiles, and microseismicity [*Melnick and Echtler, 2006; Melnick et al., 2008*]. Clusters of shallow seismicity (2-25 km depth) [*Bohm et al., 2002; Haberland et al., 2006*] occur in the forearc along these crustal faults (Figure 1). In the Arauco bay, the NE-striking and seaward-dipping Santa María reverse fault is rooted in the interplate zone and reaches a depth of 2 km from the surface, where it propagates an anticline [*Melnick et al., 2006a*]. Focal mechanisms indicate mainly reverse slip with minor dextral strike-slip component along this fault [*Bruhn, 2003*]. The NW-striking Lanalhue fault system is another major deep-reaching and seismically-active structure running along the southern flank of the Nahuelbuta Range (Figures 1a and 1c). Heterogeneous focal mechanisms of shallow events along the Lanalhue fault system have been attributed to forearc fragmentation and stress distribution [*Haberland et al., 2006*]. A Permian mylonitic shear zone is associated to this regional-scale fault system, which bounds two main basement units, leading *Glodny et al. [2008]* to characterize it as an inherited, crustal-scale feature of the margin.

The Liquiñe-Ofqui fault zone (LOFZ) is a major active strike-slip system that straddles the volcanic arc of south-central Chile, accommodating oblique plate convergence [e.g., *Lavenu and Cembrano, 1999; Rosenau et al., 2006*] (Figure 1a). The forearc sector adjacent to the LOFZ has been described as a northward translating sliver -the Chiloé block- decoupled from stable South America, as shown by geological [*Rosenau et al., 2006*] and

GPS data [Wang *et al.*, 2007]. In the Arauco-Nalhuebuta block, deformed Pliocene and Pleistocene sediments, patterns of fission-track ages, and folded Pleistocene marine terraces indicate margin-parallel shortening [Melnick *et al.*, 2008]. This shortening has been interpreted as a result of northward motion of the Chiloé block, which is bounded at its northern, leading edge by the Lanalhue fault.

3. Methods

3.1. GPS observation

We present horizontal GPS velocities from 16 new campaign sites, 3 of them originally installed in the frame of the SAGA network [Klotz *et al.*, 2001], and 3 continuous GPS stations operated by the TIGO Observatory and the University of Concepción. The sites were observed up to nine times over a 4-year time span (Table 1). Each site was occupied for at least 48 consecutive hours, but preferentially for 72 hours.

GPS data was processed using the Bernese Software Version 5.0. Processing strategies were adopted from the double-difference processing routine of Dach *et al.* [2007]. Satellite orbits and weekly Earth rotation parameters were introduced from the global solution of the Center for Orbit Determination in Europe (CODE, Analysis Center of IGS) [Schaer *et al.*, 2006]. The double difference ambiguities were resolved using the quasi-ionosphere-free strategy by processing the baselines separately. The site coordinates were estimated together with troposphere parameters, 12 Zenith path delays per day, and one set of horizontal gradient parameters per day. Processing of our campaign network included seven IGS stations, three of them (BRAZ, KOUR and LPGS) located in the stable part of the South American continent (i.e., cratonic shield in Brazil and Argentina). In a first step, daily normal equations without constraints on the coordinates were calculated. In

a second step, daily normal equations were combined and site velocities were estimated. The solutions were obtained by a No-Net-Translation condition imposed on the ITRF2000 reference coordinates and velocities [Altamimi *et al.*, 2002]. The daily repeatabilities of the coordinates for subsequent epochs were in the range of 1-2 mm. In a third step, the site velocities were calculated with respect to a stable South American reference frame. For this calculation, the Euler vector of the stable part of the South American continent was derived with respect to the ITRF2000 reference. We obtained the final vectors by subtracting the stable-South American angular velocity from the ITRF2000 velocities of our data. The reference frame is defined with precision better than 1 mm for the horizontal components.

Our final solution was combined with previously published velocities in the study area [Klotz *et al.*, 2001; Ruegg *et al.*, 2008]. In order to make both data sets compatible, we transformed the ITRF2000 velocity solutions of Ruegg *et al.* [2008] to our South American reference frame. This transformation was based on the same approach used for the datum definition of our velocities and results in a horizontal precision better than 1 mm/yr.

In order to further explore our data, we calculated the principal horizontal axes of infinitesimal strain using the `grid_strain` Matlab program [Teza *et al.*, 2008]. The strain was computed over a regular grid of 0.5° size. Rotations with respect to a downward positive vertical axis with clockwise positive sense were computed from the modeling residuals with the software SSPX [Allmendinger *et al.*, 2007].

3.2. Finite element modeling

3.2.1. Modeling setup

Interseismic deformation and the effect of a crustal fault were modeled with the finite element method (FEM) using the ANSYS[®] Academic Research, v. 11.0 software. The advantage of this method is its flexibility; it can incorporate complex geometry structures and heterogeneous material properties.

The three dimensional spherical models are constrained by kinematic boundary conditions (Equation in Appendix A). Models include topography and bathymetry [*Smith and Sandwell, 1997*] and the best available geometry of the slab and continental Moho based on the forward modeling of the gravity field of *Tassara et al. [2006]*. In our study region, this modeling used geometrical constraints given by seismic reflection and refraction profiles [*Krawczyk et al., 2006; Groß et al., 2007*], as well as microseismicity and tomography derived from local seismological networks [*Haberland et al., 2006; Lange et al., 2007*], and material properties given by surface geology [*Sernageomin, 2003*].

Our FEM models are composed of 10-node tetrahedral-shaped elements. These elements have a quadratic displacement behavior, and are well suited to model irregular meshes. Element size is between 1 and 5 km in the fault zones and 10 km in the rest of the upper crust, whereas in the oceanic crust and mantle it is 10 and 50 km, respectively (Figure 2a).

The models extend from 76-60° W to 35-45° S and to a depth of ~500 km, in order to omit boundary effects. The models consist of an elastic upper plate, an elastic subducting plate, and a viscoelastic mantle (Figure 2a). The thickness of the elastic oceanic plate is set to 30 km [*Watt and Zhong, 2000*]. We specified a Young's modulus of 100 GPa, 120

GPa and 160 GPa, for the oceanic, continental, and mantle layers, respectively, following *Hu et al.* [2004]. The Poisson ratio is set to 0.25 for the entire rock system, as adopted by similar model studies in the region [*Khazaradze et al.*, 2002; *Hu et al.*, 2004; *Wang et al.*, 2007]. The mantle viscosity is assumed to be 2.5×10^{19} Pa s following the sensitivity results from *Hu et al.* [2004].

Interseismic deformation is simulated using the back-slip method [*Savage*, 1983]. In this approach a virtual slip in a reverse sense to the plate motion is imposed on the fault interplate. We implemented this method using the split-node technique [*Melosh and Raefsky*, 1981], which allows to introduce fault displacements into FEM simulating the double-couple acting on the fault. We assume that the seismogenic zone of the plate interface is fully locked following previous studies in the region [*Klotz et al.*, 2001; *Khazaradze et al.*, 2002; *Ruegg et al.*, 2002; *Hu et al.*, 2004; *Ruegg et al.*, 2008; *Wang et al.*, 2007]. Thus, we imposed the amount of plate convergence during one year (6.6 cm) as the back slip value, using the 3D vectors estimated from plate kinematic models along the strike of the plate interface. We introduced the calculated vectors to each pair of nodes in the interplate locked zone using linear constraint equations, defined for example for the displacement component in the X direction by:

$$D_X = \sum_i^N [(R(i)) \times U_X(i)] ; \text{ where } U_X(i) \text{ is the displacement in the X direction of the node}(i), R(i) \text{ is the displacement ratio between each node in a pair of nodes on the plate interface and } D_X \text{ is the constant magnitude of the applied displacement, in this case the X component of the plate convergence rate.}$$

The applied boundary conditions of our model are schematically shown in Figure 2b. Each node on the contact faces is duplicated. Green and blue nodes, which are part of the

continental and oceanic plates, respectively, are initially located at the same coordinates. The nodes are forced to remain on the fault and consequently can only slide along the interface. After applying the constraint equations, nodes at both sides of the fault are equally displaced but in opposite directions.

The seismogenic part of the plate interface consists of a fully locked area bounded by up- and downdip transition zones (Figure 2b). The downdip transition zone extends 10 km vertically below the locked zone and the slip tapers linearly to zero. Outside the transition zone, each pair of nodes on the interface is coupled together sharing the same degrees of freedom. Above the updip limit, nodes can slip freely along the interface. Displacements perpendicular to each boundaries of the model were fixed to zero. The upper surface of the model is assumed to be stress-free, and therefore no constraints were applied.

We must emphasize that the solutions to our modeling problem are nonunique. The major uncertainties may be associated to: (1) errors in the geometry of the subduction zone, which are rarely reported in the geophysical data that we have used and difficult to estimate; (2) the degree of plate coupling and its along- and across-strike variability [e.g., *Chlieh et al.*, 2008]; and (3) heterogeneity in material properties. We adopt conservative estimates for these parameters following previous modeling studies that have used similar techniques.

3.2.2. Crustal fault modeling

In a second step, we introduced the effect of the Santa María fault on the interseismic model. We model this fault based on its documented active behavior, its relatively well-known subsurface geometry [*Bookhagen et al.*, 2006; *Melnick et al.*, 2006a] and on the residuals of the interseismic model (results in section 4.2.1). The Santa María fault is

modeled as a blind fault, which extends from the interplate zone to a depth of 2 km (Figure 2a), as constrained by seismicity and seismic reflection profiles.

The fault plane is introduced by contact-target surface elements [Saeed, 2007]. Following the split-node fault technique, we define the fault as two planes with identical distribution of nodes. Constraint equations are applied to introduce the slip rate on the fault. Contact-target elements obey the Coulomb friction criteria; surfaces can accumulate shear stresses up to a certain magnitude before they start sliding (Equations in Appendix B). The contact algorithms use the penalty stiffness method, with a contact option for closed gap, penetration reduction, exclusion of initial geometrical effect and no separation [Saeed, 2007]. Thus, contact elements are prevented from penetrating the target surface but permitted to slide along the fault.

3.2.3. Sensitivity analysis

Sensitivity analyses were performed for the unknown input parameters of the FEM modeling using probabilistic and optimization methods. For the probabilistic method, we used the Monte Carlo simulation, from which the variability of the input parameters and their influence on the results were determined. The sensitivity results are collected in the correlation matrix of the input parameters versus the output variables. An optimization analysis was performed in order to estimate the best values of the unknown input parameters, which minimize the root-mean square (RMS) between the model results and the GPS vectors.

In the interseismic sensitivity analysis, the margin was divided into 0.5-degree-long segments, in which different depths of up- and downdip limits and continental Young's

modulus were explored. In the models that included a crustal fault, the slip rate of the fault and its coefficient of friction were defined as unknown input parameters.

4. Results

4.1. GPS velocities

GPS site velocities calculated with respect to a stable South American reference frame are shown in Figure 3 and Table 1. The data cover the entire onshore forearc of the south-central Chile margin between 36 and 39.5° S. In the northern part of the Arauco-Nahuelbuta block, GPS vectors are nearly parallel to the direction of plate convergence and their magnitudes progressively decrease toward the arc. The sites on the hanging wall of the Santa María fault have the highest margin-normal velocities of up to 40 mm/yr, diminishing to 30 mm/yr at sites 30 km inland on the footwall (Figure 4). In contrast, the margin-parallel velocity of hanging wall sites is lower with respect to the counterparts in the footwall. Principal shortening axes are roughly perpendicular to the Santa María fault, decreasing abruptly in magnitude away from the fault (Figure 3).

In general, GPS vectors on the southern part of the Arauco-Nahuelbuta block have lower magnitudes than their counterparts to the north. In the proximity of the Lanahue fault, vectors have heterogeneous magnitudes and orientations (Figures 3 and 4). The coastal sites have the highest margin-normal velocities of 32 mm/yr, which decrease rapidly inland to 18 mm/yr across a distance of only 10 km. An opposite effect is observed in the margin-parallel velocities, which decrease from 20 to 12 mm/yr between Mocha Island and the mainland.

The differences in the surface velocity field along the part of the forearc under investigation permit to define two distinct sectors, the northern and southern domains. The

boundary of these two domains is located in the center of the Arauco Peninsula at 37.5° S (Figure 3).

4.2. Modeling result

4.2.1. Interseismic model result

A comparison between the velocities predicted by the best-fit interseismic model and the GPS vectors is shown in Figure 5a. The model vectors agree relatively well with the GPS velocities in the northern domain, but large discrepancies appear in the southern sector. The average RMS is 3.15 mm/yr and 14.11 mm/yr in the northern and southern domains, respectively. GPS velocities are successfully reproduced by the interseismic model along the cross section at 37.2° S (Figure 5b). In this profile, a downdip depth of 46 km produces the lowest RMS of 2.19 mm/yr. A shallower downdip depth results in slower surface velocities, whereas a deeper limit leads to faster rates. Sensitivity results suggest that the downdip depth of the interplate locked zone has the most significant influence on the interseismic surface velocity field, whereas variations in the Young's modulus have a minor effect. A value of 100 GPa for the continental Young's modulus provided the lowest RMS (Figure 5c). The updip transition affects mostly coastal sites and has a weak influence on the rest of the sites.

Our results imply that the locked portion of the seismogenic zone is wider in the northern domain, where the depth of the downdip limit shallows gradually southward from 49 to 45 km (Figure 6). A depth of 12 km for the updip limit was our best estimate in this domain. Because of the heterogeneity of GPS vectors in the southern domain, we relied on geophysical estimates of the up- and downdip limits based on the distribution of microseismicity and tomographic models derived from local seismic networks [*Haberland*

et al., 2006; *Lange et al.*, 2007], and from seismic reflection and refraction profiles [*Groß et al.*, 2007]. We adopted a downdip depth of 44 km at 38° S, which decreases to 40 km at 42° S. Between 42 and 45° S, the downdip depth was set to 35 km following *Lange et al.* [2007]. The depth of the updip limit was fixed at 10 km based on the onset of microseismicity for the entire southern domain [*Haberland et al.*, 2006; *Lange et al.*, 2007].

Two areas have significant residual velocities (Figure 7a). The first area is the northern coastal region in the proximity of the Santa María fault, where several sites have SW-directed residual vectors with an average RMS of 4.26 mm/yr. The second area is in the southern domain of the Arauco-Nahuelbuta block; here high magnitude residuals are directed seawards and rotate progressively in a counterclockwise sense (Figure 7b).

4.2.2. Fault model results

The interseismic model that includes the Santa María fault provides a better fit to the GPS observations. The average residual velocities of the near-fault sites decrease from 4.26 mm/yr to 2.70 mm/yr after including the crustal fault (Figure 8a). Fault deformation produces the surface velocity gradient observed in the GPS vectors near this structure (Figure 8b). Our sensitivity results suggest that the strike-slip rate along the Santa María fault has a significant effect on the surface velocity. Vertical slip rate and the coefficient of friction have a secondary effect, with a significance of about 40% with respect to the horizontal slip (Figure 8c). We obtained a dextral strike-slip rate of 6.9 mm/yr, and a reverse dip slip rate of 2.8 mm/yr. A coefficient of friction of 0.6 was the best estimate for the fault.

5. Discussion

Our new GPS data show that forearc deformation exhibits heterogeneous patterns in the Arauco-Nahuelbuta block. GPS displacements can be grouped in two sectors: the northern and southern domains, which follow the rupture boundaries of two recent megathrust earthquakes: the 1835 ($M \sim 8.5$) Concepción and the 1960 (M_w 9.5) Valdivia events.

In the northern domain, GPS vectors are generally parallel to each other and to the direction of plate convergence, and their magnitude decrease continuously inland. This pattern has been previously interpreted as to reflect locking of the plate interface during the interseismic phase of the earthquake cycle [Klotz *et al.*, 2001; Ruegg *et al.*, 2002]. The residual velocity field after subtraction of the interseismic model velocities from our GPS observations shows an anomalous pattern in the coastal sites between the Santa María Island and Concepción (Figure 7a). Here, residuals are oriented parallel to the Santa María fault and reach maximum values of ~ 6 mm/yr. This suggests that the Santa María fault is active during interseismic period, as previously proposed based on the occurrence of a cluster of crustal seismicity along the fault [Melnick *et al.*, 2006a]. Our best-fit model including this fault in addition to locking of the megathrust incorporates vertical and dextral horizontal fault slip rates of 2.8 and 6.9 mm/yr, respectively, and a coefficient of friction of 0.6 (Figure 8c). This value of friction is in agreement with laboratory estimates [Byerlee, 1978].

Our GPS data in the entire northern domain show shortening, which we attribute to locking of the plate interface, and thus ongoing thrust-type shear of the upper plate by megathrust loading. Because no megathrust earthquakes have ruptured the Concepción segment since 1835, loading is expected to be in an advanced phase, which might promote

thrust faulting. Thus, activity of the Santa María fault at present may be releasing part of the interseismic stress accumulated since the last great earthquake rupture.

In the southern domain, GPS vectors vary markedly in orientation and magnitude, with a much lower degree of correlation with the interseismic pattern than that observed in the northern domain (Figures 3 and 4). Based on regional GPS data and FEM models, this area has been previously interpreted as influenced by prolonged postseismic mantle rebound following the 1960 earthquake [*Khazaradze et al.*, 2002; *Hu et al.*, 2004].

In the northern limit of the 1960 earthquake rupture zone, the residual velocities of the interseismic model exhibit an heterogeneous pattern. Residual vectors situated north of the Lanalhue fault rotate in a clockwise mode, whereas to the south of the fault residuals rotate counterclockwise (Figure 7b). Their dissimilar magnitude and direction may result from the boundary effects between postseismic and interseismic deformation. In addition, heterogeneous mantle rebound could follow patches of variable slip during the 1960 earthquake resulting in complex patterns of surface velocity. However, modeling these processes would require detailed knowledge of the 1960 slip distribution and will be the scope of further work.

An alternative interpretation of the counterclockwise rotation pattern of residual velocities in the northern limit of the 1960 earthquake rupture may arise from a detailed inspection of regional tectonic features and fault geometries. The 1960 rupture zone seems to be coincident with the extent of the Chiloé forearc sliver, which translates parallel to the margin decoupled from stable South America by the Liquiñe-Ofqui fault zone [*Melnick et al.*, 2008] (Figure 9). The convergence between the Chiloé forearc sliver and the Arauco-Nahuelbuta block is accomodated by folding and thrusting in the Arauco Peninsula as

well as by oblique thrusting along the Lanalhue fault [*Melnick et al.*, 2008]. Because of the oblique, NW strike of the Lanalhue fault, the northern leading edge of the Chiloé block is a triangular region expected to rotate counterclockwise as a result of margin-parallel sliver translation. In contrast, regional GPS data [*Klotz et al.*, 2001; *Wang et al.*, 2007] as well as finite-element models [*Khazaradze et al.*, 2002; *Hu et al.*, 2004; *Wang et al.*, 2007] show that rotations arising from postseismic mantle rebound at the northern limit of the 1960 earthquake rupture are dominantly clockwise and extend over a broad region between the forearc and the back-arc. Thus, because the counterclockwise rotations observed in the GPS vectors occur exclusively in a limited region between the coast and the Lanalhue fault, they may be caused by the collision of the Chiloé sliver against the Arauco-Nahuelbuta block. This collision appears to be partly accommodated by the Lanalhue fault (Figure 9).

Our model results suggest that the interplate coupling zone narrows southward along the south-central Chile margin (Figure 6). In the northern domain, the downdip limit of coupling reaches a depth of 49 km at 36° S shallowing to 45 km at 37.5° S. These values are in agreement with the intersection of the slab with the continental Moho, determined independently by tomography [*Bohm et al.*, 2002; *Haberland et al.*, 2006], seismic reflection and refraction profiles [*Lüth et al.*, 2003; *Krawczyk et al.*, 2006; *Groß et al.*, 2007], and modeling of gravity data [*Tassara et al.*, 2006]. In the southern domain, the downdip limit is at 44 km depth at 38° S and shallows to 40 km at 42° S. This change in downdip depths between the 1835 and 1960 earthquake-rupture segments is likely a result of the gradual variation in age of the incoming plate along the trench. As slab age decreases southward, heat-flow increases resulting in narrower coupling [*Wang et al.*, 2007]. Our

statistically-calculated updip limit for the northern domain is consistent with a depth of 12 km, which coincides with the prediction of *Grevenmeyer et al.* [2003] based on heat-flow measurements.

Along the 1960 rupture zone segment, the margin-parallel component of oblique plate convergence is partly accommodated by the LOFZ [*Rosenau et al.*, 2006]. GPS data show that this structure absorbs about 30% of the margin-parallel component [*Wang et al.*, 2007]. However, across the northern limit of the 1960 segment, where the LOFZ terminates and where our GPS data show counterclockwise rotations in the coastal region, the degree of strain partition along the margin decreases considerably. This gradient in the degree of partitioning has been deduced from changes in the kinematics of Quaternary faults along the fore-, intra-, and back-arc regions [*Melnick et al.*, 2006b] (Figure 9). Our modeling results for the Santa María fault suggest a dextral strike-slip rate of 6.8 mm/yr, which given its strike would result in about 6 mm/yr of margin-parallel motion, equivalent to about 25% of the margin-parallel component of plate convergence. This would support the previous proposition of a gradient in the degree of strain partitioning: in the southern 1960 earthquake domain, part of the margin-parallel component is accommodated along the intra-arc zone by the LOFZ; whereas in the northern 1835 earthquake domain, lower magnitudes of margin-parallel motion are distributed across several faults located in the forearc, such as the Santa María fault, as well as in the intra- and back-arc domains, thus suggesting a lower degree of partitioning.

6. Conclusions

New GPS data have revealed heterogeneous deformation patterns along the south-central Chile forearc. Variations are spatially correlated with the rupture limits of the

two past megathrust earthquakes, the 1835 $M \sim 8.5$ Concepción and 1960 M_w 9.5 Valdivia events. Finite-element models of interseismic deformation including complex crustal geometries, constrained by various geophysical data sets, are unable to fully reproduce the heterogeneous GPS deformation patterns. In the northern 1835 earthquake domain, interseismic models that include the Santa María fault, a crustal-scale reverse/dextral structure, better reproduce the GPS observations. In the southern domain, in turn, the interseismic model residuals show counterclockwise rotations, which could reflect either postseismic relaxation of the mantle at the northern edge of the 1960 rupture zone or activity of the seismically-active Lanalhue fault, or both.

Our study suggests that crustal-scale faults rooted in the interplate seismogenic zone may affect the surface deformation field during the interseismic phase of the earthquake cycle. This effect, though local, might have a significant amplitude. We propose that these structures may release part of the contractional strain that accumulates during interseismic locking of the megathrust, affecting the surface velocity field. Thus, active faults rooted in the plate interface should be considered when inverting geodetic data to constrain locking depths of the seismogenic zone.

Appendix A: Elastic equation

The elastic behavior of the oceanic and continental crust, respectively, is described by:

$$\operatorname{div} \sigma = -\underline{f},$$

where $\sigma(\underline{u}) = \lambda \operatorname{tr}(\epsilon(\underline{u})) \operatorname{id} + 2\mu \epsilon(\underline{u})$ is the stress, \underline{f} the volume force,

$\epsilon(\underline{u}) = (\nabla \underline{u} + (\nabla \underline{u})^T)/2$ the strain, and λ and μ the Lamé constants. The Young's modulus and Poisson's ratio are expressed as $E = \frac{\mu(3\lambda+2\mu)}{\lambda+\mu}$ and $\nu = \frac{\lambda}{2(\lambda+\mu)}$, respectively.

Appendix B: Contact interface

For the contact let g denote the gap between two surfaces, then the contact pressure F_n reads:

$$F_n = \begin{cases} t_n - e_n \cdot g & : g < 0, \\ t_n \cdot e^{-e_n/t_n \cdot g} & : g \geq 0, \end{cases}$$

where t_n estimates the contact force and e_n is the penalty stiffness. The force for the Coulomb friction reads:

$$F_f = \begin{cases} K \cdot u_t & : K \cdot u_t \leq \mu \cdot F_n \text{ (sticking)}, \\ \mu \cdot F_n & : K \cdot u_t > \mu \cdot F_n \text{ (sliding)}, \end{cases}$$

where u_t is the tangential displacements, μ the friction coefficient, and K the sticking stiffness.

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Table 1. GPS station locations and calculated horizontal velocities

| ID | Longitude | Latitude | V_e mm/yr | 1σ error | V_n mm/yr | 1σ error | Correl. coeff | Num. Surveys | Time Epochs |
|------|-----------|----------|----------------|--------------------|----------------|--------------------|------------------|-----------------|----------------|
| AROA | -72.771 | -36.736 | 28.5 | 1.37 | 10.3 | 1.19 | -0.45 | 9 | 2002.6-2005.4 |
| CACH | -73.211 | -36.772 | 34.4 | 1.26 | 9.4 | 2.01 | -0.66 | 4 | 2002.8-2007.0 |
| CLAS | -72.668 | -39.285 | 13.9 | 1.80 | 3.7 | 1.09 | -0.38 | 2 | 2003.9-2005.9 |
| IMOR | -73.664 | -37.723 | 19.1 | 1.67 | 17.6 | 2.20 | -0.70 | 5 | 2003.9-2007.1 |
| LAJA | -72.52 | -37.256 | 25.7 | 2.74 | 3.9 | 0.55 | -0.21 | 3 | 2003.9-2007.0 |
| LEBU | -73.668 | -37.596 | 34.8 | 0.47 | 16.0 | 0.13 | -0.66 | 4 | 2003.9-2007.1 |
| MOCH | -73.905 | -38.410 | 32.9 | 1.52 | 8.1 | 2.12 | -0.70 | 6 | 2002.7 -2007.1 |
| NACI | -72.689 | -37.607 | 18.0 | 2.56 | 4.6 | 0.54 | -0.31 | 4 | 2002.8-2007.1 |
| NAHU | -73.031 | -37.824 | 15.6 | 2.78 | 8.6 | 0.24 | -0.74 | 3 | 2003.9-2007.1 |
| STJU | -72.849 | -37.206 | 28.2 | 2.31 | 7.2 | 1.37 | -0.79 | 2 | 2003.8-2007.0 |
| STCL | -72.361 | -36.836 | 28.6 | 2.25 | 4.8 | 0.70 | -0.55 | 3 | 2003.8-2007.0 |
| STDO | -73.546 | -37.023 | 40.1 | 1.90 | 12.1 | 2.61 | -0.69 | 4 | 2004.1-2007.1 |
| STCA | -73.53 | -37.059 | 38.8 | 1.07 | 10.8 | 1.84 | -0.66 | 4 | 2004.1-2007.1 |
| TIRU | -73.502 | -38.341 | 19.1 | 2.82 | 12.3 | 1.08 | -0.45 | 4 | 2003.9-2007.1 |
| TOLT | -73.182 | -39.349 | 17.9 | 1.90 | 7.1 | 2.53 | -0.58 | 3 | 2002.8-2005.9 |
| VARA | -73.238 | -38.531 | 19.2 | 1.66 | 8.5 | 0.83 | -0.69 | 2 | 2003.8-2005.9 |
| CONZ | -73.026 | -36.844 | 31.9 | 1.79 | 8.8 | 1.38 | -0.48 | Permanent Site | Since 2002 |
| HUAL | -73.189 | -36.746 | 38.6 | 1.31 | 10.9 | 0.39 | -0.71 | Permanent Site | Since 2005 |
| UDEC | -72.344 | -37.472 | 21.4 | 1.67 | 6.9 | 0.48 | -0.56 | Permanent Site | Since 2006 |

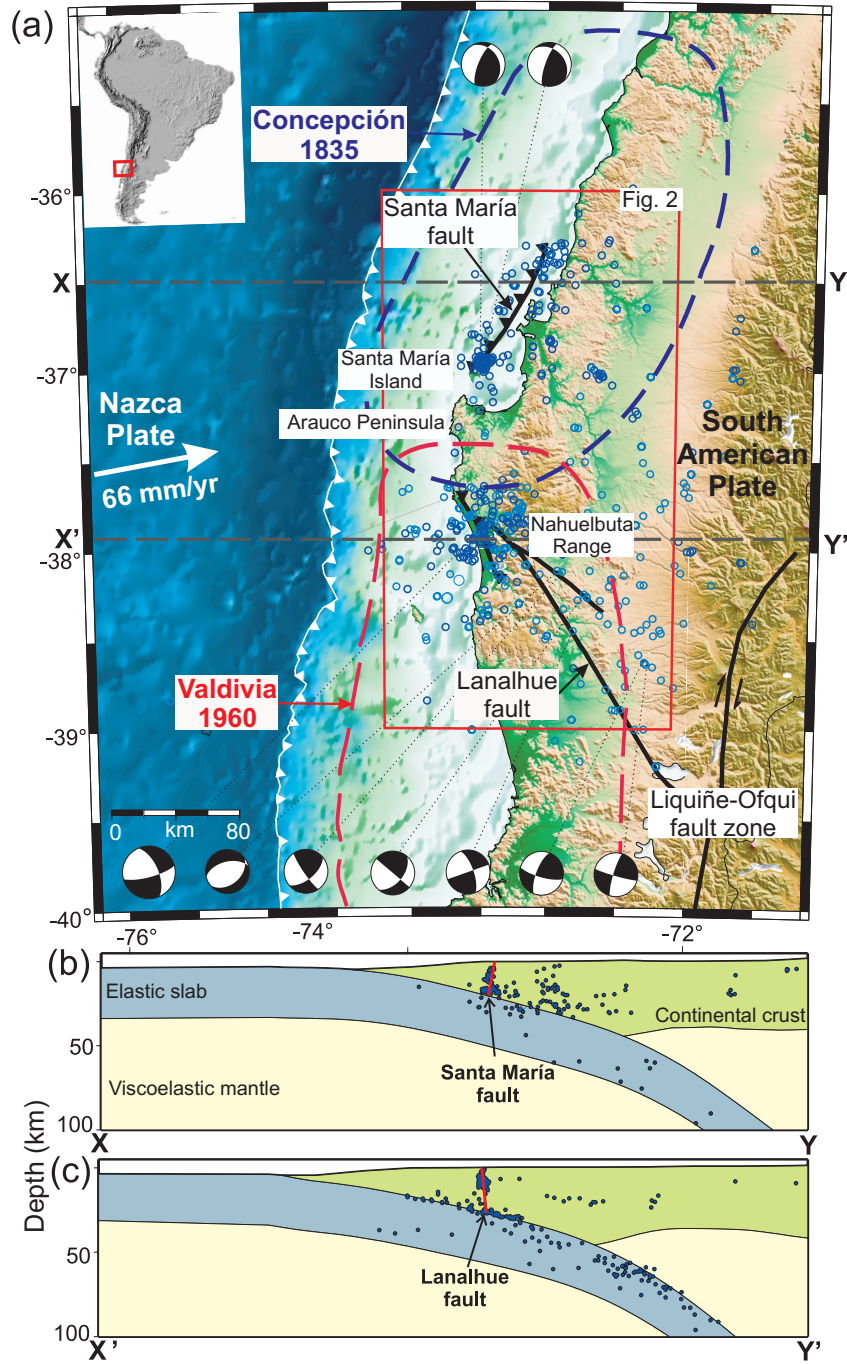


Figure 1. (a) Main tectonic features of the south-central Chile margin. Red box shows the Arauco-Nahuelbuta forearc region. Dotted blue and red lines define the rupture zones of the 1835 and 1960 megathrust earthquakes, respectively [Lomnitz, 2004]. Local seismicity is depicted by open circles [Bohm et al., 2002; Bohm, 2004; Haberland et al., 2006]. Focal mechanisms are from Bruhn [2003] and Haberland et al. [2006]. (b-c) Profiles at 36.5° and 38° S showing cluster of aligned seismicity along the Santa María and Lanalhue faults, respectively.

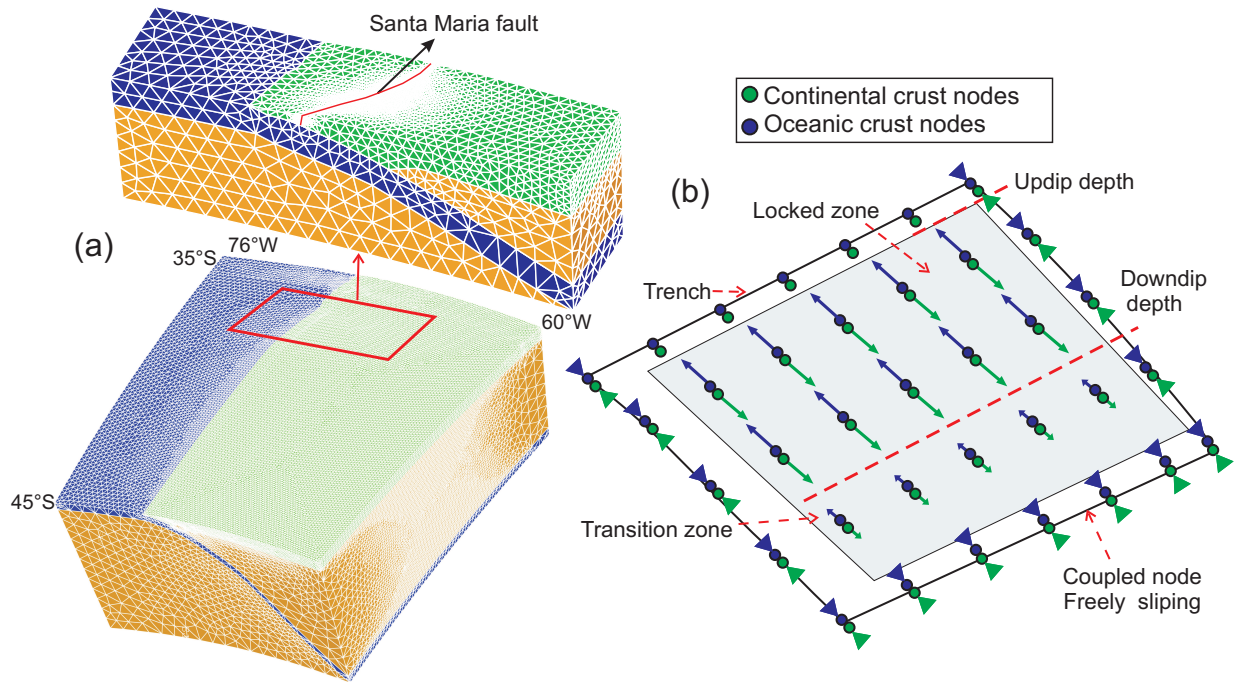


Figure 2. (a) 3-D finite element model setup. Green, blue and orange elements represent the continental and oceanic lithosphere, and mantle, respectively. Extracted portion of the mesh shows detail along the Santa María fault. (b) Schematic representation of nodes in the plate interface. Arrows depict how constraint equations simulate the double-couple acting on the fault.

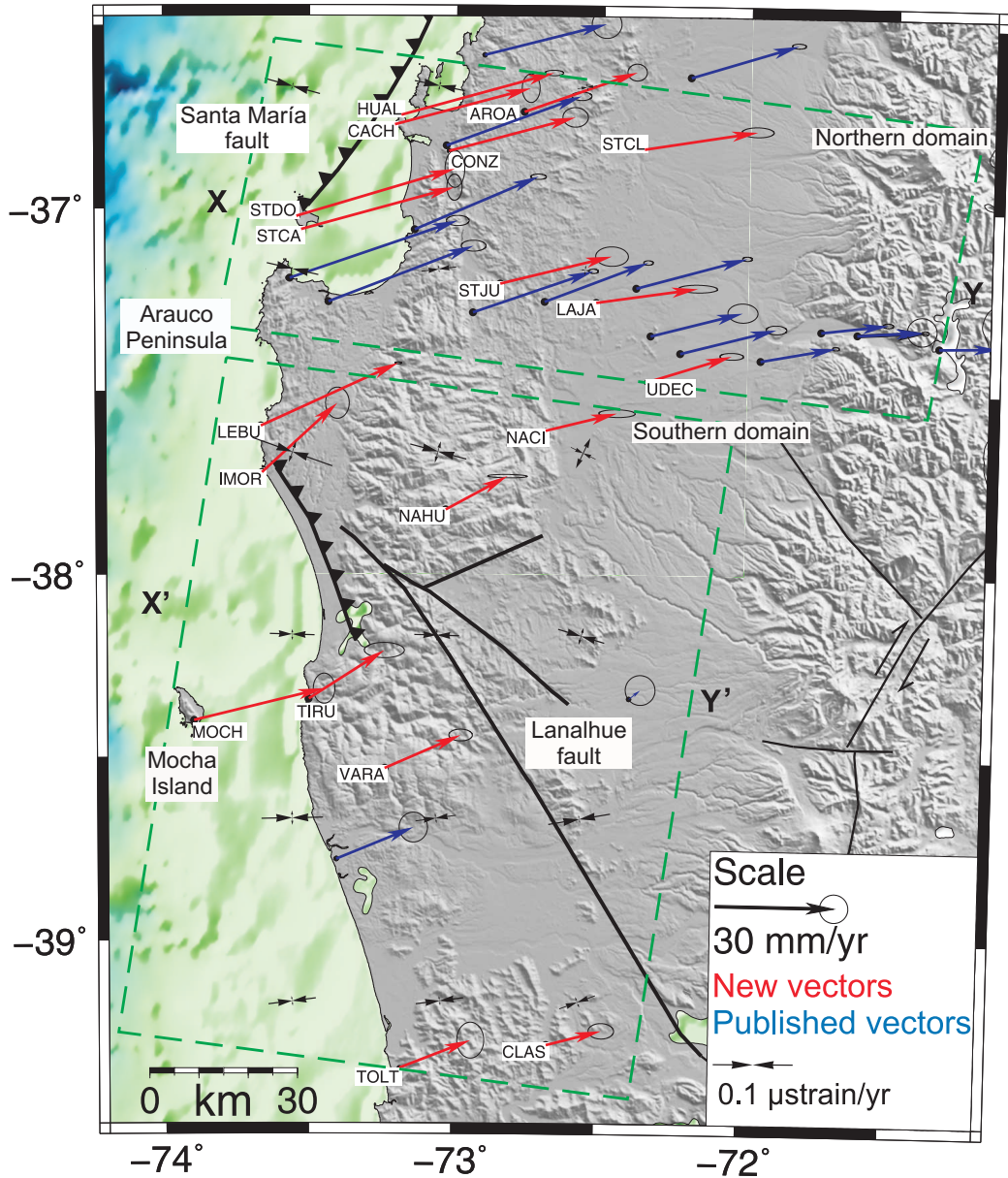


Figure 3. GPS velocity vectors of the south-central Chile forearc relative to a stable South American reference frame. Ellipses represent 95% confidence limits. New GPS velocities presented in this paper are shown in red (Table 1), velocities by *Klotz et al.* [2001] and *Ruegg et al.* [2008] are shown in blue. Principal axes of infinitesimal horizontal strain are depicted by black crosses. The green dotted boxes denote the northern and southern domains, and areas of profiles XY and X'Y' shown in Figure 4.

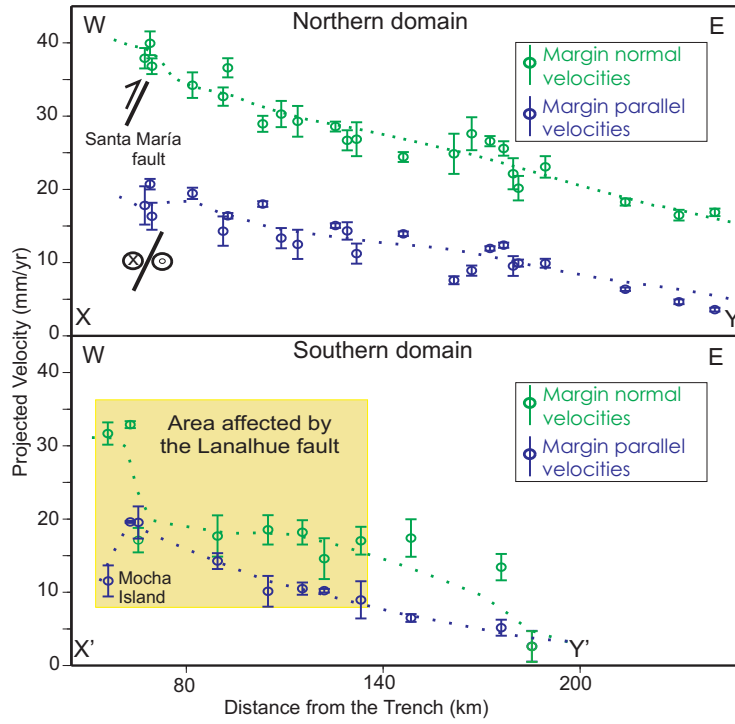


Figure 4. Horizontal GPS velocities from profiles projected normal (blue) and parallel (green) to the margin. Location of profiles in Figure 3. In the northern domain, the Santa María fault is depicted by a solid line. Reverse and dextral-strike slip motion on the fault are indicated.

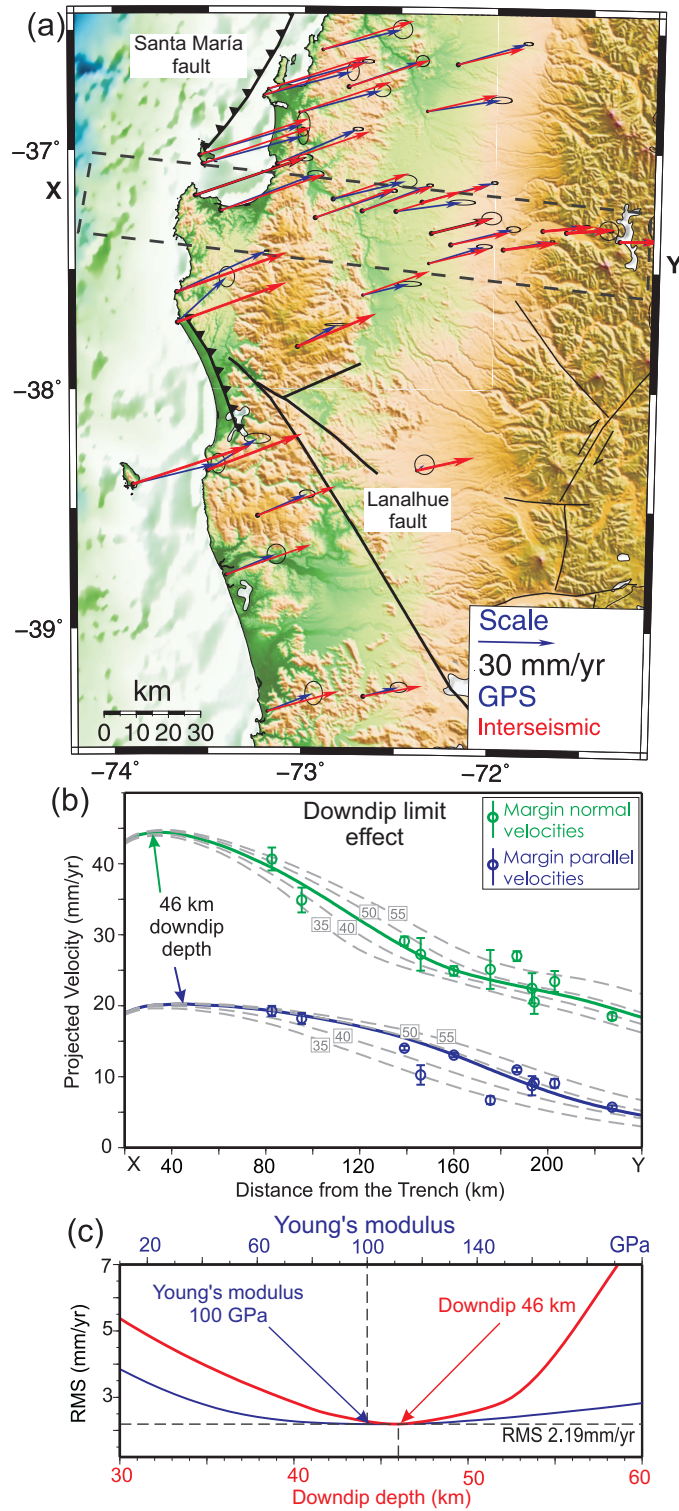


Figure 5. (a) Comparison of the GPS vectors (blue) with the velocities of the interseismic model (red). (b) Margin normal cross section at 37.2° S. Interseismic model results for different downdip depth limits are plotted. (c) RMS response to downdip depth, and continental Young's modulus variations (See text for details).

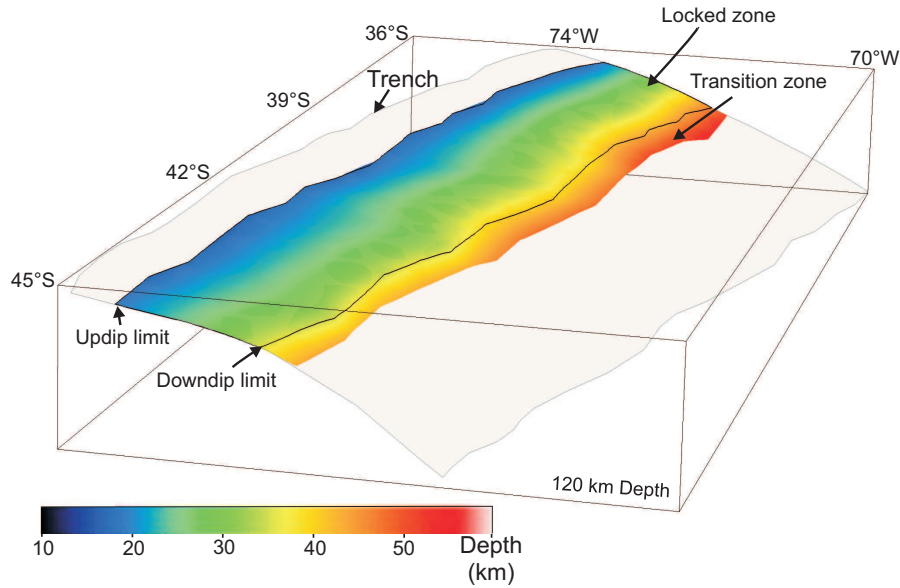


Figure 6. Up- and downdip depth limits of the coupling zone used in our FEM modeling. Below the downdip limit, a 10-km linear transition from fully-coupled to zero slip was applied. The seismogenic zone is wider on the northern part, where it reaches a depth of 49 km. This zone gradually shallows to 35 km depth at 45 °S

(See text for details).

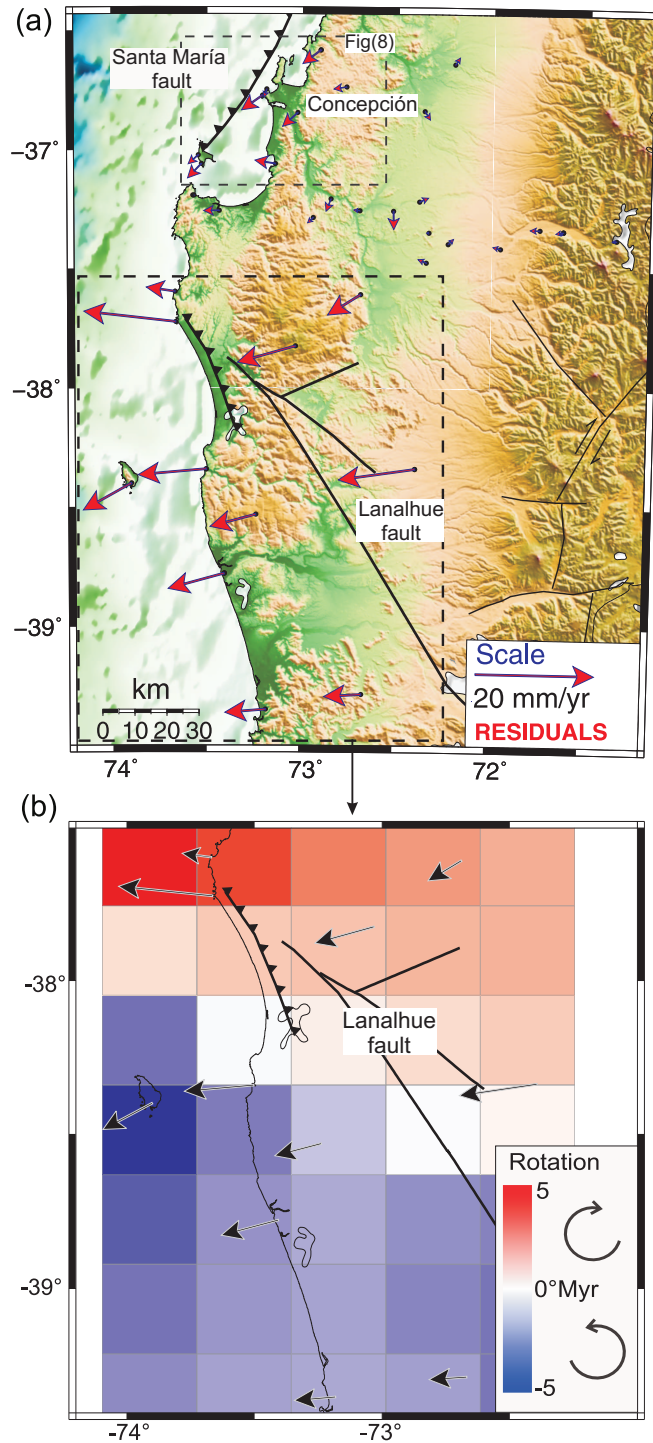


Figure 7. (a) Residual velocities obtained by subtracting the interseismic model from the GPS velocities. (b) Vertical-axis rotation from the interseismic residuals on the southern domain, calculated with the software SSPX [Allmendinger *et al.*, 2007] over a regular grid of 30 km.

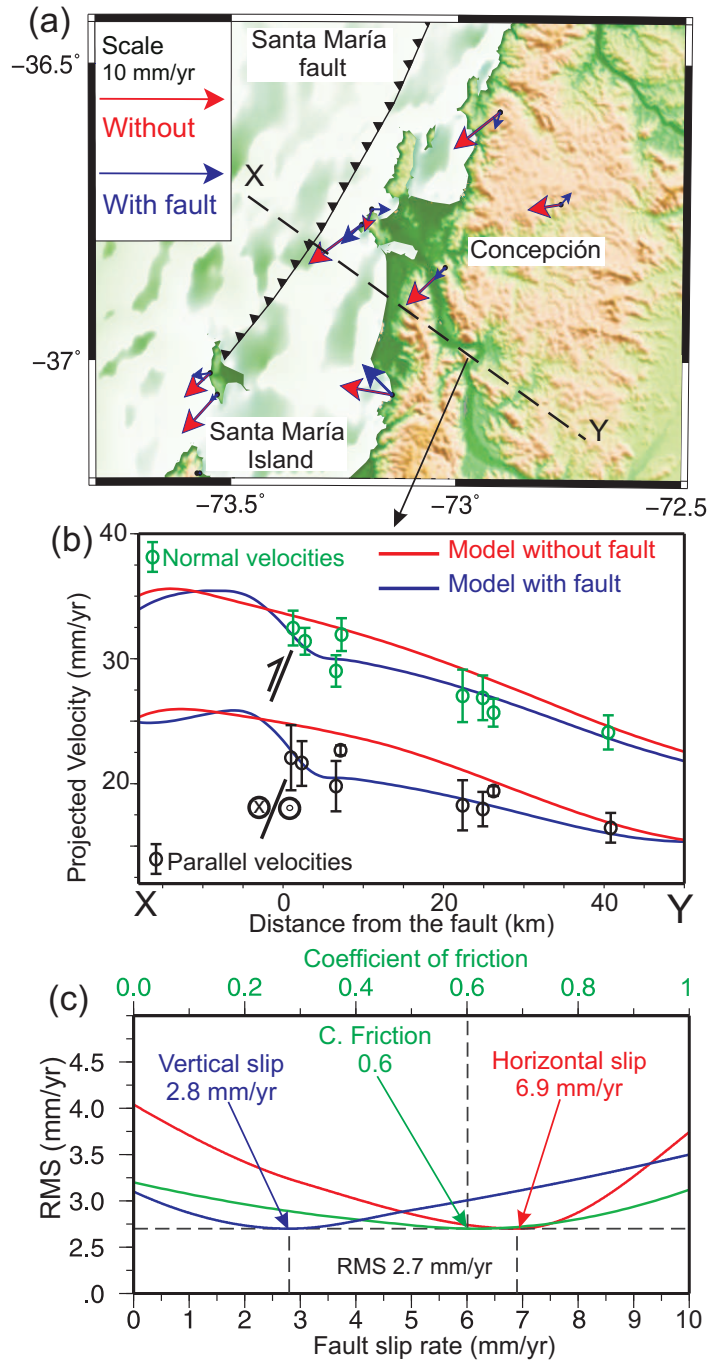


Figure 8. (a) Residuals after subtraction of deformation caused by the interseismic deformation and effect of Santa María fault. (b) Cross section XY normal to the Santa María fault. Interseismic model results with and without effects of the fault are shown. Fault-related deformation extends up to 35 km from the fault, and may be responsible for the velocity gradient observed in the GPS vectors. (c) RMS response to changes fault slip and friction coefficient. The horizontal fault slip has the principal effect on the RMS.

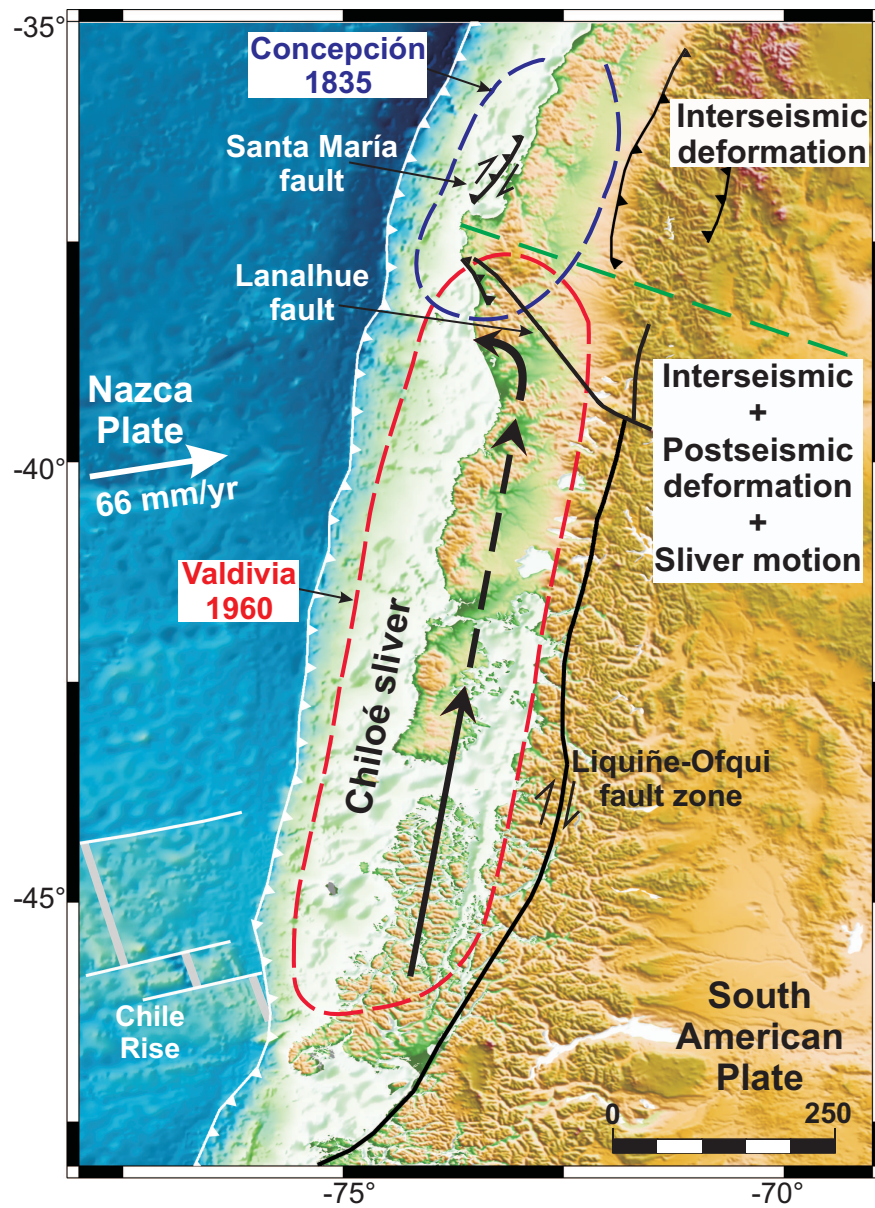


Figure 9. Schematic map showing the main tectonic features that may control the deformation in the south-central Chile margin (See text for details).