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1 **Cost effective monitoring of ground motion related to earthquakes,**  
2 **landslides or volcanic activity by joint use of a single-frequency GPS**  
3 **and a MEMS accelerometer**

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7  
8 **Key points:** (1) Joint processing of GPS and accelerometer data. (2) GPS velocity  
9 estimate using the broadcast ephemeris. (3) Monitoring of strong ground motion by  
10 combined low-cost sensors.

11 **Abstract:** Real-time detection and precise estimation of strong ground motion are  
12 crucial for the rapid assessment and early warning of geohazards such as earthquakes,  
13 landslides and volcanic activity. This challenging task can be accomplished by  
14 combining GPS and accelerometer measurements because of their complementary  
15 capabilities to resolve broadband ground motion signals. However, for implementing  
16 an operational monitoring network of such joint measurement systems, cost-effective  
17 techniques need to be developed and rigorously tested. We propose a new approach  
18 for joint processing of single-frequency GPS and MEMS-type accelerometer data in  
19 real time. To demonstrate the performance of our method, we describe the results  
20 from free-field experiments. For validations, we analyzed the dual-frequency GPS  
21 data and images recorded by a video camera through post-processing. The results of  
22 the different sensors agree very well, suggesting that real-time broadband information  
23 of ground motion can be provided by using single-frequency GPS and MEMS-type  
24 accelerometers.

25 **Index terms:** 7212, 1240, 1241, 7294, 8419

26

## 27 **1 Introduction**

28 Displacements associated with earthquakes and volcanic activity may span  
29 multiple scales, from sub-millimeter per year to tens of meters within seconds [Segall,  
30 2010]. Similarly, landslides and ice sheet motions are also multi-scale. Rapid  
31 detection and quantification of this multitude of displacement scales is challenging,  
32 and commonly approached by combining various technical concepts. However, many  
33 of these displacements may involve accelerations on the order of  $10^{-5}$  to  $10 \text{ m/s}^2$ . For  
34 technical reasons, the scales of deformation are often not fully detected, and the  
35 processes remain poorly understood.

36 In recent years, high-rate GPS technology has been continuously improved and  
37 increasingly useful to explore large displacements and accelerations [Bilich et al.,  
38 2008; Larson, 2009; Blewitt et al., 2009]. However, a well-known limitation of  
39 high-rate GPS is that its high precision can only be guaranteed in the low frequency  
40 band. For frequencies larger than a few hertz, the GPS data involves generally large  
41 uncertainties caused by environmental and instrumental noise [Genrich and Bock,  
42 2006]. In comparison, digital accelerometers can measure the strong ground shaking  
43 with a much higher resolution than the GPS, but their records usually include  
44 so-called baseline errors, which are induced dominantly by ground tilting. Though  
45 these errors are generally very small, they affect seismometer records in the low  
46 frequency band and thus prevent retrieving the true ground velocity and displacement  
47 from the recorded accelerograms [Boore, 2001]. In previous studies, baseline errors of

48 accelerometer sensors were corrected using empirical methods, which generally  
49 involve uncertainties that are not easily quantified without a geodetic reference [Wang  
50 et al., 2011].

51 Many approaches have suggested an integrated analysis of high-rate GPS and  
52 accelerometer data [Emore et al., 2007; Bock et al., 2011; Wang et al., 2013]. In most  
53 cases, the displacement data from a nearby GPS station is used as the reference to  
54 optimize the empirical baseline correction of the accelerometer records. To improve  
55 cost-effectiveness of co-located devices, we propose a different approach for the  
56 integrated analysis. In this approach, the site velocity is estimated using carrier phase  
57 observations of a single-frequency GPS receiver with satellite orbits and clocks from  
58 the broadcast navigation information that is decoded from the received satellite  
59 signals [Colosimo et al., 2011]. Therefore, it can be performed independently of the  
60 station and has good timeliness. In general, most of the errors can be modeled precisely  
61 [Dach et al., 2007] and atmospheric delays and biases in the satellite orbits and clocks  
62 can be significantly reduced by using epoch-differentiated observations [Colosimo et  
63 al., 2011]. However, the remaining atmospheric errors, satellite clock and orbit biases,  
64 multipath effects, and high-frequency noises are still remarkable. Such remaining  
65 errors result not only in high-frequency noises, but also a slow trend in the estimated  
66 velocity time series. According to Colosimo et al. [2011], the slow trend can be  
67 approximated to be linear for a short time period (e.g., a few minutes). For  
68 seismological observations, for example, such linear trends can be estimated through  
69 least squares regression of the data within an appropriate pre-event time window. The

70 trend-corrected GPS velocity can then be integrated to displacement. Presently, the  
71 high-rate GPS displacement seismograms obtained in this way have an accuracy of a  
72 few centimeters [Colosimo et al., 2011].

## 73 **2 Method**

74 For cost-effectiveness, the event-trigger mode may be used to monitor strong  
75 ground motion events. In this mode, such events can be detected by using a threshold  
76 approach based on the accelerometer records, as done by a seismic early warning  
77 network [see, e.g., Fleming et al., 2009]. In practice, detection of the end of a ground  
78 motion event (such as an earthquake) is usually more complicated because of coda  
79 waves that may decay slowly but without producing any permanent ground  
80 deformation. We propose to consider that a ground motion event is over when the  
81 ground acceleration has decreased below 10% of its PGA (peak ground acceleration)  
82 for a long enough time (e.g., as long as the pre-event time window).

83 Once a ground motion event is detected, the joint data processing is performed in  
84 three steps. First, an appropriate pre-event time window (10-20 s) is chosen. Within  
85 the pre-event window, the ground motion is considered negligible. Thus, the initial  
86 linear trend in the GPS and the initial offset in the accelerometer baseline can be  
87 determined independently and will be removed from their respective data streams.  
88 Second, the trend-corrected GPS velocity is integrated into the GPS-based  
89 displacement, which provides the reference for the accelerometer-based displacement,  
90 so that the baseline shift in the accelerometer record can be derived by comparing the  
91 two displacement datasets. Finally, broadband ground motion information (time series

92 of displacement, velocity and acceleration) are derived from the baseline corrected  
 93 accelerometer record.

94 Define  $V_G$  as the real-time GPS velocity estimation based on the broadcast  
 95 ephemeris and epoch-difference measurement [Colosimo et al., 2011] since an initial  
 96 time  $t = 0$ , prior to the detected event start, denoted as  $t_0$ . Through a linear  
 97 regression within the pre-event time window  $[0, t_0]$ , we can estimate the initial trend  
 98 in  $V_G$  given by  $\alpha_0 + \beta_0 t$  and extrapolate it to the whole event period. After  
 99 correcting for this initial trend, we calculate the GPS-based displacement time history  
 100 by integration,

$$U_G(t) = \int_0^t [V_G(\tau) - (\alpha_0 + \beta_0 \tau)] d\tau. \quad (1)$$

101 On the other hand, we obtain the accelerometer-based displacement time history  
 102 by double integration of the accelerometer records, defined as  $A_S$ ,

$$U_S(t) = \int_0^t \int_0^\tau [A_S(\xi) - A_0] d\xi d\tau, \quad (2)$$

103 where  $A_0$  represents the pre-event baseline offset of the accelerometer sensor.

104 Recognizing the complementary advantage of the two measuring instruments, we  
 105 may suppose that the time series  $U_G(t)$  and  $U_S(t)$  can be expressed in the form,

$$U_G(t) = u(t) + G_{noise}(t) \quad (3)$$

106 and

$$U_S(t) = u(t) + S_{trend}(t), \quad (4)$$

107 where  $u$  is the true ground displacement,  $G_{noise}$  represents the high-frequency noise  
 108 included in the GPS-based displacement data, and  $S_{trend}$  represents the

109 low-frequency trend in the accelerometer-based displacement data caused by the  
110 event-induced baseline errors.

111 Without using the GPS data,  $S_{trend}$  has to be estimated empirically. To use the  
112 GPS and accelerometer data jointly, we introduce a residual time series between  $U_S$   
113 and  $U_G$ ,

$$U_{dif}(t) = U_S(t) - U_G(t) = S_{trend}(t) - G_{noise}(t), \quad (5)$$

114 so that  $S_{trend}$  and  $G_{noise}$  can be estimated by the low-pass and high-pass filters  
115 applied to  $U_{dif}$ , respectively. In our approach, we determine  $S_{trend}$  by smoothing  
116  $U_{dif}$  through a moving Gaussian window with a bandwidth of 1-2 seconds and then  
117 the true ground displacement  $u$  is calculated by subtracting  $S_{trend}$  from  $U_S$ ,

$$u(t) = U_S(t) - S_{trend}(t). \quad (6)$$

118 As  $S_{trend}$  can be interpolated and even extrapolated for a short time, the time series  
119  $u$  of the accelerometer sampling rate can be achieved, although the trend can only be  
120 estimated using the GPS and accelerometer data at the common epochs. The true  
121 ground velocity and acceleration are obtained by differentiating  $u$  over time.

122 In order to validate the low-cost combination, dual-frequency GPS and camera  
123 video data were analyzed through post-processing, as described in the next section.

124

### 125 **3 Free-field experiment**

126 Figure 1 shows the sledge that we used in several free-field experiments carried  
127 out in December 2012. The sledge, which can move along a table, includes a dynamic  
128 GPS antenna, a low-cost MEMS accelerometer [Fleming et al., 2009] and a

129 high-precision accelerometer (CMG-5T Compact made by Guralp Systems Ltd). The  
130 sampling rate is 50 Hz for the GPS and 100 Hz for the two accelerometer sensors. The  
131 maximum sliding distance of the sledge was restricted to about 0.5 m in one direction.  
132 A video camera recorded the motion of the sledge from a distance of 10 m at 25 fps  
133 (frames per second). The images, with a constant pixel resolution of 3 mm, were  
134 analyzed by manual identification of the sledge and automatic image-to-image  
135 tracking using a Normalized Cross Correlation code [Walter, 2011].

136 We use the aforementioned joint data processing approach in simulated real-time  
137 mode for the single-frequency (L1) GPS data and accelerometer records. For  
138 illustration purposes we show a selected experiment, in which the sledge is shifted  
139 stepwise from 0 to 0.3 m. The final results of other experiment examples are  
140 summarized at the end of this section. Figure 2 shows the sledge velocity obtained  
141 from the single-frequency GPS carrier observation and the acceleration from the  
142 MEMS accelerometer records. For simplicity, the pre-event trend in the GPS velocity  
143 time series and the initial offset in the accelerometer records have been removed. To  
144 show the complementary information involved in the two different measurements, all  
145 differentiated and integrated time series are given in Fig. 2 as well.

146 Although the GPS velocity data and the derived acceleration seem noisy, the  
147 integrated displacements reflect an uncertainty of a few centimeters, compared with  
148 the dual-frequency GPS and camera results (Fig. 3c) as reference. In contrast, the  
149 original accelerometer-based acceleration and velocity (after the empirical baseline  
150 correction) have a much higher signal-to-noise ratio. From the post-event trend of the



151 accelerometer-based velocity data (Fig. 2e), we can derive the permanent baseline  
152 shift of the accelerometer sensor to be  $0.004 \text{ m/s}^2$ , which can be explained by a tilt of  
153  $0.024^\circ$  of the sledge after the experiment, causing the gravity to be projected in the  
154 horizontal direction ( $0.004 \text{ m/s}^2 \approx 9.8 \text{ m/s}^2 \times \sin 0.024^\circ$ ). Though this baseline shift  
155 accounts for only a few per thousandth of the peak acceleration, we observe that it is  
156 impossible to obtain the displacement through double integration of the original  
157 accelerometer record. The displacement time history shown in Fig. 2f is calculated by  
158 using the empirical baseline correction suggested by Wang et al. [2011]. This time  
159 series clearly exhibits two kinks resulting from the bi-linear approximation used for  
160 the baseline correction. Without the baseline correction, no displacement signal could  
161 be visible at all because of the large trend.

162 For the combined data processing, the lower sampling rate of the two  
163 measurement systems, which is 50 Hz in the present case, is used for estimating the  
164 trends. Fig. 3a shows that the residual time series  $U_{dif}$  dominates the rapid trend in  
165 the accelerometer-based displacement time series. Subtracting the smoothed  $U_{dif}$ ,  
166 which we obtained by using a moving Gaussian window of 2 s (i.e., 100 epochs),  
167 from the accelerometer-based displacement  $U_S$  (black curve in Fig. 2f), we calculate  
168 the true displacement and velocity time series shown in Fig. 3b and c, respectively.  
169 Particularly, Figure 3b shows that the stepwise sliding signals of the experimental  
170 sledge have been clearly resolved with a bias less than 2-3 cm using the real-time  
171 combined data processing approach, validated by the camera (25 Hz) measurements  
172 and the results of the dual-frequency GPS obtained using the PPP approach through

173 post-processing. In Fig. 3c, the velocity time series derived from the camera images is  
174 also shown, and the amplitude appears systematically larger than that from the  
175 low-cost combination. We explain this discrepancy by the limited pixel resolution of  
176 the camera (3 mm), leading to an overestimate of the velocity peaks. Notice that the  
177 camera-based velocity also shows stochastic noise on the same order of the  
178 overestimate.

179 In Fig. 4, we summarize the results from the combined data processing for the  
180 other seven free-field experiments. For each experiment, the post-event part of the  
181 combined GPS and accelerometer data is used to evaluate the uncertainty of the  
182 low-cost measurement system. In all experiments, the displacement deviations of the  
183 combined system are within 2-3 cm, using the dual-frequency GPS and camera results  
184 as reference. Note that we also tested the proposed procedure using the records by the  
185 Guralp sensor instead of the MEMS sensor, but found no substantial difference in the  
186 retrieved velocity and acceleration time series. This observation verifies the finding  
187 by Picozzi et al. [2011] that, for frequencies over 0.5 Hz, there is no significant  
188 difference between the response spectra between the MEMS and Guralp sensors that  
189 we used in this study.

190

#### 191 **4 Discussion and conclusions**

192 We have proposed and tested a simple, but sophisticated, approach to integrate  
193 co-located high-rate GPS and accelerometer measurements. Based on our free-field  
194 experiments, the real-time accuracy of the combined system for the horizontal

195 displacement is on the order of 2-3 cm, validated by the dual-frequency GPS and  
196 camera observations.

197 Note that when processing a ground motion event, the same broadcast ephemeris  
198 record has to be used during the whole event period to avoid possible jumps in the  
199 results due to the discontinuity of adjacent ephemeris records. Additionally, we  
200 emphasize that we have performed the combination of the two measurements in the  
201 displacement domain. In principle, it seems that the procedure also works in the  
202 velocity domain. However, the key achievement of the joint use is to estimate the  
203 low-frequency trend in the residual data between the accelerometer and GPS-based  
204 time series. The trend is strongly amplified through this integration and therefore can  
205 be determined more precisely in the displacement domain than in the velocity domain.  
206 Another point to be mentioned is the choice of the low-pass filter used to separate the  
207 accelerometer-based trend from the GPS-based noise. We have used the Gaussian  
208 smoothing window, which corresponds to an acausal low-pass filter because it covers  
209 the same length (1 s or 50 epochs) of past and future data. Due to the 1 s time delay,  
210 the tool that we have presented here is, strictly speaking, applicable for the  
211 near-real-time joint data processing.

212 In addition, the new method estimates the GPS velocity using the broadcast  
213 ephemeris received from the satellite signals directly, so that it has a better timeliness.  
214 In summary, our experimental results have shown that the combined system of a  
215 single-frequency GPS and a MEMS accelerometer is able to monitor broadband  
216 ground motion with precision satisfying most current demands in real-time

217 seismology and earthquake engineering, with potential applications in other fields as  
218 well.

219

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225

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## Figure captions

Figure 1. A sketch of the experiment sledge consisting of a GPS receiver, a video camera, a low-cost accelerometer of the MEMS (SM1) and a high-precision accelerometer of the Guralp (SM2).

Figure 2. Sledge acceleration, velocity and displacement based on the single-frequency GPS (panels a-c) and MEMS accelerometer data (panels d-f). The original velocity derived from the GPS carrier observations and acceleration from the MEMS accelerometer records are plotted in (b) and (d), respectively. The bi-linear red curve in (e) represents the empirical correction of the event-induced trend in the accelerometer-based velocity time series.

Figure 3. Results from the combined processing of the GPS and accelerometer data for the selected experiment. a) Residual time series  $U_{dif}$  between the accelerometer- and GPS-based displacement time series. b) Displacement time series  $u$  retrieved by subtracting the smoothed  $U_{dif}$  from the accelerometer-based displacement, validated by the dual-frequency GPS (blue) and camera results (red). c) Velocity time series  $v = du/dt$ , compared with the camera observations.

Figure 4. Results from the other seven experiments. Left column: Displacement time series retrieved using the combined processing of the GPS and accelerometer data, validated by the results from the dual-frequency GPS (blue) and camera observations

(red). Middle column: Velocity time series obtained by differentiating the corresponding displacement time series. Right column: Acceleration time series given by the records of SM1.









