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1	Hyperspectral and Lidar intensity data fusion: A framework for the		
2	rigorous correction of illumination, anisotropic effects and cross-		
3	calibration		
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14 Abstract

15 The fusion of hyperspectral imaging sensor (HSI) and airborne lidar scanner (ALS) 16 data provides promising potential for applications in environmental sciences. Standard 17 fusion approaches use reflectance information from the HSI and distance 18 measurements from the ALS to increase data dimensionality and geometric accuracy. 19 However, the potential for data fusion based on the respective intensity information of 20 the complementary active and passive sensor systems is high and not yet fully 21 exploited. Here, an approach for the rigorous illumination correction of HSI data, based 22 on the radiometric cross-calibrated return intensity information of ALS data, is 23 presented. The cross-calibration utilizes a ray tracing-based fusion of both sensor measurements by intersecting their particular beam shapes. The developed method is 24

25 capable of compensating for the drawbacks of passive HSI systems, such as cast and 26 cloud shadowing effects, illumination changes over time, across track illumination and partly anisotropy effects. During processing, spatial and temporal differences in 27 illumination patterns are detected and corrected over the entire HSI wavelength 28 domain. The improvement in the classification accuracy of urban and vegetation 29 surfaces demonstrates the benefit and potential of the proposed HSI illumination 30 31 correction. The presented approach is the first step towards the rigorous in-flight fusion of passive and active system characteristics, enabling new capabilities for a variety of 32 applications. 33

Keywords: airborne laser scanning (ALS); de-shadowing; imaging
 spectroscopy; in-flight; mosaicking; pixel-level fusion; pre-processing;
 radiometric alignment; ray tracing; sensor alignment, sensor fusion;

37 **1 Introduction**

38 Data fusion is a promising approach for producing remote sensing data sets with improved quality and dimensionality. The combination of data from airborne 39 hyperspectral imaging sensors (HSIs) and airborne lidar scanners (ALSs) has been 40 41 previously addressed in the literature [1], [2], [3], [4], [5], [6], [7], [8]. The particular 42 focus is their complementary sensor characteristics, yielding increased data 43 dimensionality and improved classification. The combination of the high spectral resolution of the HSI and the structural information provided by the ALS can yield more 44 45 complete and improved surface characteristics for a wide range of applications.

Fusion processes are complex, and there are different methods and levels of detail to achieve data-type combinations. All approaches rely on an accurate geometric coalignment of both data sources [9]. In general, fusion methods are categorized as either physical or empirical approaches [10]. Physical approaches aim to combine both

sensors on a raw data level. Their focus is a parametric representation of particular 50 rigorous sensor models, as well as external conditions. In contrast, empirical 51 approaches combine both data sets based on inherent, observable information, 52 53 without the need for supplementary information. Most approaches, whether physical or empirical, focus on the enhancement of information content by adding the surface 54 elevation information, ALS point classification, and spatial-statistic information as 55 additional dimensions. Additionally, physical approaches consider exclusively 56 57 structural and geometric information [11], [12]. However, ALS systems are not limited to this specific information content. Similar to HSI systems, they also provide intensity 58 59 information, but usually only for a single ALS wavelength. In contrast, the intensity information is acquired actively and is unfortunately not internally calibrated. Due to 60 the different sensor characteristics, the combination of intensity information is 61 62 challenging and has often not been taken into account. Several recent studies [13], [14], [15] systematically compare data from both intensity information sources and note 63 64 both opportunities and challenges for the adaptation of both sensor responses for heterogeneous surfaces. An overview of the benefits of using the LAS intensity 65 information is given in [16]. Nevertheless, the full use of data from both imaging 66 sensors requires some type of radiometric cross-calibration. A cross-calibration 67 between HSI and ALS creates a consistent relative radiometric calibration scale, in 68 69 which the ALS intensities are converted to physical units through comparison with the calibrated HSI data. This process ensures and enhances the temporal, spatial and 70 71 spectral comparison of two different sensor systems and is, in addition to the geometric 72 alignment, one of the essential steps for comprehensive data fusion.

The purpose of this sensor fusion is to compensate for solar illumination and atmospheric conditions, as well as directional and shadow effects, to derive improved and realistic at-surface reflectance. This is achieved by the rigorous radiometric

calibration of the ALS intensity data with the HSI data and the subsequent correction
of the amount of direct solar radiation within the atmospheric correction of the HSI data.
We have designed and implemented new software for efficient HSI and ALS fusion,
with special focus on the radiometric calibration of ALS intensity data and HSI
illumination correction. Detailed descriptions of the basics, methodology, results and
discussion are provided in this paper.

82 2 Background

83 2.1 Radiative transfer characteristics

The two sensors have different radiation transfer paths, individual spatial sampling and sensor characteristics. Therefore, the alignment of different sensor characteristics on a raw level requires a physical radiative transfer-based cross-calibration. Fig. 1, in combination with Table 1, provides an overview of the different radiative transfer paths and interactions with the exposed surfaces of the two sensor systems.



89

91

90 Fig. 1: Conceptualization of the radiative transfer paths of ALS and HSI sensors. See

Table 1 for notification and symbol explanations.

Notation	Explanation	Units
E_0	Terrestrial solar irradiance	[W/m ²]
$ au_s$	Atmospheric transmittance sun-surface	[]
$ au_{atm}$	Atmospheric transmittance surface-sensor	[]
E_{dir}	Direct radiation	[W⋅sr ⁻¹ ⋅m ⁻²]
E_{dif}	Diffuse radiation	[W⋅sr ⁻¹ ⋅m ⁻²]
E_{adj}	Adjacency radiation	[W⋅sr ⁻¹ ⋅m ⁻²]
L_{HSI}	Electromagnetic intensity measured by the HSI	[W⋅sr ⁻¹ ⋅m ⁻²]
L_p	Path radiance	[W⋅sr ⁻¹ ⋅m ⁻²]
Θ_s	Solar zenith angles	[deg]
$oldsymbol{eta}_{sol}$	Solar incidence angle	[deg]
$ heta_{HSI}$	Viewing angle of the HSI	[deg]
d	Relative sun-to-earth distance	[]
P_t	Emitted pulse intensity of the ALS	[dB]
P_r	Backscattered laser pulse of the ALS	[dB]
α_{ALS}	Incidence and viewing angle of the ALS	[deg]

94 The atmospheric conditions influencing the measured signals are not the same due to their different atmospheric transfer paths (see Fig. 1). Thus, atmospheric conditions 95 96 (e.g., cirrus and clouds) above the flight level influence only the HSI transfer path. In 97 addition to cloud shadowing, HSI radiances are influenced by cast shadows, introducing a continuous shadow field exclusively illuminated by diffuse radiation (E_{dif} 98). Compared to direct irradiation, diffuse radiation caused by scattering is not a discrete 99 100 status and is strongly spectrally variable and dependent. For example, the blue parts 101 of the spectrum are scattered more strongly, and they are thus represented 102 significantly more strongly in the cast shadow [17]. However, lidar intensities are not 103 influenced by the cast shadow due to their active character. This enables active cast 104 shadow detection and correction with a physical approach based on the overlapping 105 wavelength domain and the proportional assignment to the remaining wavelength 106 range of the HSI sensor system.

In general, airborne spectroscopy attempts to identify the true reflectance or absorption
property of a surface object at the bottom of the atmosphere (BOA). However, the

electromagnetic intensity (L_{HSI}) measured by HSI sensors is influenced by the solar illumination (terrestrial solar irradiance (E_0) and solar zenith angles (Θ_s)), its path through the atmosphere (atmospheric transmittance τ_s) starting at the top of the atmosphere (TOA), its incidence angle from the object (β_{sol}) , its path back through the atmosphere (τ_{atm}) to the sensor at flight level and the resulting path radiance (L_p) (Fig. 1). The HSI BOA surface reflectance (ρ_{HSI}) of a Lambertian surface can be modelled as:

116
$$\rho_{HSI} = \frac{\pi d^2 (L_{HSI} - L_P)}{\tau_{atm} (E_{dir} + E_{dif})}.$$
 (1)

117 The different terms in Eq. 1 are listed in Table 1. The diffuse radiation (E_{dif}) also 118 includes spherical atmospheric albedo reflected from the surface towards the sensor 119 and adjacency radiation (E_{adj}). The direct radiation (E_{dir}) can be calculated by:

 $E_{dir} = E_0 \tau_s \cos \Theta_s \,. \tag{2}$

121 In addition, surface roughness and anisotropic object properties are also relevant for122 the radiative transfer.

123 Without geometric and morphometric information of the surface object, HSI data can 124 only be corrected to Lambertian-equivalent reflectance, where directional effects and 125 shadows are not taken into account.

Alternately, a large advantage of ALS data is that the surface normal (n) of an object surface can be calculated by the analysis of neighbouring point measurements, enabling the reconstruction of the incidence angle of the laser pulse. This circumstance can also be exploited within the radiometric calibration of ALS intensity data. Several studies devote themselves to the absolute radiometric calibration of ALS data [18], [19], [20] and a review of lidar radiometric processing is given in [21]. Most approaches rely on the basic lidar equation (3) and substitution of unknown terms with ground-based in-situ reflectance measurements:

134
$$P_r = \frac{P_t D_r^2}{4\pi R^4 \beta_t^2} \tau_{sys} \tau_{atm} \sigma \,. \tag{3}$$

135 In general, the measured backscattered laser intensity is analogous to HSI systems 136 influenced by sensor parameters, atmospheric conditions and surface properties. The backscattered laser pulse (P_r) is the result of the emitted pulse intensity (P_r) and its 137 138 direction, range (R) or path through the atmosphere and return, its atmospheric transmittance (τ_{atm}) , and the effective target cross-section (σ) considering the 139 incidence angle (α_{ALS}). Sensor-dependent parameters (e.g., the beam width angle (140 141 β_t), receiver aperture size (D_r), and system transmittance factor (τ_{sys}) describing 142 sensor specific attenuation, such as the transmittance efficiency and sensitivity of the 143 detector) and basic sensor specifications (e.g., wavelength, bit depth, multiple 144 returns/full-waveform, an amplifier for low-reflectivity surfaces, attenuation for near 145 targets and automatic gain control) are required. Additional overall influential factors are solar background radiation and the size, angle of incidence, roughness and 146 147 wetness of the illuminated surface. Usually, the emitted pulse intensity, some sensor 148 parameters, and the atmospheric conditions are unknown. Rigorous approaches 149 assume that these parameters are constant over the entire flight campaign. Thus, they 150 can be represented by a calibration constant (C_{cal}), which can be estimated by in-situ 151 reflectance measurements [19], [12]. Based on the lidar equation (3) for every return 152 signal, the backscatter coefficient (γ_i) can be calculated. The backscatter coefficient is independent of range (R) and beam divergence (β_{i}) because it is normalized to the 153 154 laser's transverse area [18], [19].

155 3 Methodology

156 The proposed approach is the first step towards an in-flight, physically based fusion of 157 airborne radiometric measurement capabilities by combining an active ALS sensor with a passive HSI sensor. Most of the influential parameters are wavelength-dependent, 158 159 and the overlapping wavelength domain thus defines the comparability of the sensor responses. The data fusion is performed by intersecting the pointing of a HSI sensor 160 161 element, represented by a cone, with the ALS point cloud. Hence, the complete set of ALS point properties inside one HSI beam can be accessed and adequately adapted, 162 considering the full radiometric and structural information. 163

164 The complete in-flight radiative transfer-based cross-calibration of the ALS and HSI 165 intensity signal can be split into three principal parts (see Fig. 2):

- Input data acquisition and pre-processing (including the geometric co-alignment
 of the sensors)
- Cross-calibration and BOA reflectance calculation
- Output data generation



Fig. 2. Overview of the simplified cross-calibration workflow (rectangles represent data
products; processing procedures are represented by rhombs; yellow outlines indicate
steps applied to ALS data only; blue outlines indicate steps used for HSI data only,
grey outlines indicate levels associated with both datasets; and central fusion steps
are outlined in red).

176 3.1 Input data generation and pre-processing

177 For the purpose of developing the in-flight sensor fusion, a test dataset with a specially

178 adapted measurement setup, sensor operation, and flight planning was generated. In

addition to the HSI system, consisting of two HySpex sensors (VNIR-1600 and SWIR-

180 320m-e [22], [23]), an ALS (LMS-Q560 [24], [25]) and an IMU/GPS (AEROcontrol-IId

181 IMU in combination with a NovAtel OEM4-G2 GPS) for measuring the position and

- 182 attitude of the airplane were integrated inside a Cessna 207 Skywagon. Table 2 gives
- 183 an overview of the HSI and ALS specifications.
- 184

Table 2: Comparison of relevant sensor parameters

	VNIR and SWIR HSI (Hyspex)	ALS (LMS-Q560)
Principle	passive	active
Sensor design	Pushbroom	Whiskbroom (polygon mirror)
FOV (Field of View)	VNIR: 35.5° SWIR: 27.2°	45° (up to 60°)
IFOV (instantaneous field of view)	VNIR: across track 0.18 mrad along track 0.36 mrad SWIR: across track 0.75 mrad along track 0.75 mrad	-
Laser beam divergence		< 0.3 mrad
FWHM (spectral)	VNIR: 1.0-2 pixels SWIR: 1.5-2 pixels	
Spectral range	VNIR: 400 - 1000 nm SWIR: 1000 – 2500 nm	1550 nm (Laser class 1)
Frames per second (HSI) Pulse frequency (ALS)	VNIR: 135 fps SWIR: 100 fps	240 kHz (160 lines/s)
Spectral sampling	VNIR: 3.7 nm SWIR: 6 nm	monochromatic
Pulse length		< 4 ns at half maximum
Echo sampling interval		Full-waveform (1 ns)
Intensity digitization	12 bit	16 bit
Spectral bands	VNIR: 160 SWIR: 256	1
Spatial pixels HSI	VNIR: 1600 SWIR: 320	

185

Four flight lines were acquired at an altitude of 800 m above ground over an airfield 186 187 with bordering suburban development in Kamenz, Germany (51.29063°N 14.12107°E). The acquired suburban objects (buildings, roads, trees, fields, and 188 moving objects) represent a radiative as well as a morphometrically diverse test site. 189 190 The achieved ground sampling distances of approximately 1.2 m for SWIR and 0.6 m 191 for VNIR, as well as a point density of approximately 5 points/m² delivered by the ALS 192 in non-overlapping areas, sufficiently represent the spectral and morphological surface heterogeneity. The HSI test data are strongly influenced by cloud shadows and cast 193

shadows that limit any HSI analysis (Fig. 3 (A)). Accordingly, this test site represents
an ideal benchmark to show the capabilities and limitations regarding the fusion of
active and passive system characteristics.



197

Fig. 3: Overview of the four geocoded flight lines (1-4); HSI footprint coloured in black,
ALS footprint coloured in blue; (A) HSI SWIR radiance image (1550 nm); (B) ALS
intensity image (1550 nm).

In addition to the elevation information, ALS range, amplitude and echo width are provided to meet the requirements of the proposed method. For state-of-the-art fullwaveform ALS systems, these attributes are easily accessible.

204 The full-waveform ALS, the IMU/GPS measurement unit and the HSI (VNIR and SWIR)

205 provide the input database. The pre-processing includes the calculation of trajectories

206 (see rhomb 1 in Fig. 2), the geometric pre-processing of the ALS data including filtering

- of outliers and ALS returns introduced by atmospheric interactions (see rhomb 2 in Fig.
- 208 2), and the radiometric correction of the HSI data (see rhomb 3 in Fig. 2). Additionally,
- 209 the cross-calibration requires a proper geometric co-alignment of the HSI intensity
- 210 information with the ALS point cloud. This co-alignment of the HSI sensor data to the

ALS data is created with a parametric approach using the adapted ALS intensity information as a geometric reference. The applied approach is described in detail in [9] and also includes a detailed description of the necessary spectral response adaptation (SRF) [26], system integration, data acquisition and pre-processing. The ray tracing-based approach delivers a subpixel co-alignment in heterogeneous urban areas, as well as a look-up table (LUT) for all ALS points that intersect a particular HSI beam.

218 3.2 Cross-calibration procedure

As shown in Fig. 2 (rhomb 5), the cross-calibration itself is implemented in four major steps:

I. Calculation of incidence, illumination and viewing geometry for both sensors

II. Calculation of HSI bottom of atmosphere (BOA) reflectance at 1550 nm

223 III. Radiometric calibration of the ALS sensor

IV. Calculation of the transfer factor (X_{cross}) and HSI BOA reflectance



Fig. 4. Detailed workflow of the four cross-calibration steps. Rectangles represent input and output data products (A-D). Rhombs represent the applied processing modules (1-8).

229 3.2.1 Calculation of incidence, illumination and viewing geometry for both sensors

230 The calculation of the incidence, illumination and viewing geometry is the first step in

- the cross-calibration workflow (see Fig. 4 (I)). The ALS incidence angles (α_{ALS}), solar
- illumination angles (β_{sol}) and HSI viewing angles (Θ_{HSI}) are essential to characterize
- the interaction between the sensors and the sun with the local surface (see Fig. 1). In
- 234 general, the calculation of the angles is carried out by a ray tracing-based intersection
- of the sensor beams with the local surface model.

The ALS incidence angle (α_{ALS} , Fig. 6 (1)) is calculated in a first step by intersecting each ALS beam with its neighbouring ALS beams. The ALS beam is defined by its beam divergence, the position of the transmitter and the position of the surface target. A least squares approach fits a plain through all points that fall into one ALS beam. For every plain representing the local underlying surface that is intersected by an ALS beam, the surface normal is calculated. The angle between this ALS beam and the surface normal represents the ALS incidence angle (α_{LIDAR}).

For the calculation of the solar illumination angles (β_{sol}) (see Fig. 6 (2)), the surface 243 intersected by the HSI beams and their surface normal are calculated with the same 244 procedure used for the calculation of the ALS incidence angle. The viewing angles (245 246 Θ_{HSI} ; see Fig. 6 (3)) between the HSI beams and the surface normal are calculated, as well as the terrain slope angle (Θ_T) and the topographic azimuth angle (φ_T) . 247 Additionally, the solar azimuth (φ_s) and solar zenith angles (Θ_s) are calculated based 248 on the acquisition date and the position. By applying all these angles, the solar 249 250 illumination angle is given for every HSI beam [27]:

$$\beta_{sol} = \arccos(\cos\Theta_T \cos\Theta_s + \sin\Theta_T \sin\Theta_s \cos(\varphi_T - \varphi_s)).$$
(4)

252

253 3.2.2 HSI Bottom of atmosphere (BOA) reflectance calculation (Fig. 4 (3))

For the radiometric calibration of the ALS, the HSI BOA reflectance must be known for the overlapping wavelength domain (1550 nm). Therefore, the TOA HSI radiance data cube is transformed to BOA reflectance (Fig. 2, rhomb 5 II). This atmospheric correction is realized with in-house correction algorithms [28] [29], [26] based on the radiative transfer code MODTRAN4 [30]. Thereby, the BOA surface reflection (ρ_{HSI}) is calculated with the standard formulas (1) and (2). Shadows and rough terrain are not considered in this correction step (Fig. 6 (3)). ρ_{HSI} , E_{dir} and E_{dif} are provided separately for the overlapping wavelength domain (1550 nm), to enable the subsequent calculation of X_{cross} .

263 3.2.3 ALS radiometric calibration (Fig. 4 (4))

The calculated HSI reflectance from the previous processing step is now used for the calibration of the ALS intensity signal applying the calibration constant (C_{cal}) [19], [20], [21], [18]. Based on the lidar equation and the use of the backscatter coefficient (λ_i) [19], the surface reflectance ρ_{ALS} can be directly calculated:

268
$$\rho_{ALS} = C_{cal} \frac{R^2 P_r}{\tau_{atm} \cos \alpha_{ALS} 4}.$$
 (5)

269 The constant sensor parameters are combined into one calibration constant (C_{cal}).

270
$$C_{cal} = \frac{16}{P_t D_r^2 \tau_{sys}}$$
 (6)

To determine the calibration constant (C_{cal}), we solve equation (8) for C_{cal} :

272
$$C_{cal} = \frac{\rho_{ALS} \tau_{atm} \cos \alpha_{ALS} 4}{R^2 P_r}.$$
 (7)

Several approaches (e.g., [19], [18]) substitute ρ_{ALS} with in-situ reflectance measurements to determine C_{cal} . Instead of an empirical calibration based on the insitu reflectance measurements of surface targets, our approach aims to create an inflight cross-calibration with the wavelength overlapping HSI sensor. The criteria for every HSI beam includes that the calibration surface is a homogeneous target that can be assumed to be a Lambertian reflector representing stable radiation conditions and that it is not influenced by shadows. For the test data, which are strongly influenced by cloud shadows, an area of interest (AOI) was manually defined that covers the directly illuminated part of the runway. Within this AOI, only HSI beams were selected automatically, which have viewing angles $\Theta_{HSI} \leq 0.5^{\circ}$, intersect at a minimum with five ALS points, and have incidence angles $\alpha_{ALS} \leq 0.5^{\circ}$.

The requirement for substituting ρ_{ALS} with ρ_{HSI} in equation (7) is that the spatial response of the ALS sensor must be adapted to the spatial response of the HSI sensor. Therefore, ALS points that fulfil the mentioned criteria and intersect with the selected HSI beams are spatially adapted. The spatial response adaptation is described in 3.2.4. Therefore, both sensor responses can be regarded as analogous at this point. This adaptation is created for all HSI beams (N_{HSI}) that satisfy the mentioned criteria to calculate the mean calibration constant C_{cal} :

291
$$\overline{C_{cal}} = \frac{1}{N_{HSI}} \sum_{j=1}^{N_{HSI}} \frac{\pi d_j^2 (L_{HSI_j} - L_{P_j}) \cos \alpha_{ALS_j} 4}{(E_{dir_j} + E_{dif_j}) R_j^2 P_{r_j}}.$$
 (8)

Using $\overline{C_{cal}}$ for the radiometric calibration of the ALS intensities within equation (5) results in cross-calibrated ALS reflectances (Fig. 4 (5) and Fig. 6 (6)).

294 3.2.4 Spatial response adaptation of ALS points

To compare both sensor signals, the cross-calibrated intensity signal of the ALS point cloud has to be adapted spatially, considering the point spread function (PSF) of the HSI sensor (Fig. 4 (6)). It is created with a ray tracing-based approach intersecting the HSI cones with the ALS point cloud. The received ALS signal (P_r) is weighted relative to its distance to the cone centre with a Gaussian PSF centred along the centre axis of the HSI cone. A detailed description of the spatial response adaptation is given in [9]. With this method, the spatial response function is correctly approximated regarding the spatial footprint projection and orientation. All calculations are realized in SWIR sensor geometry (Fig. 10) and back-projected to ALS points and VNIR data. This strategy avoids the resampling of the HSI data and thus the associated degradations.

305 Due to the ray tracing-based intersection approach, a filtering and adaptation of the point cloud are created separately for every single HSI beam. The discrete return 306 307 intensities are filtered based on their elevation variance inside one HSI beam (Fig. 5). 308 Every time the elevation variation inside an HSI beam exceeds a threshold, the 309 variance is minimized by separating the point cloud into two continuous surfaces by 310 histogram filtering. This approach results in two continuous surface representations: 311 the ALS points representing higher regions in the canopy, and the bare ground points. 312 Only if sparse first pulse returns and dense higher order returns are detected inside 313 one HSI beam, the higher order returns are also considered in the sensor response 314 adaptation (Fig. 5).



- 315
- Fig. 5: Interaction between the canopy, ALS pulses (red lines; returns are indicated with numbered dots) and HSI beam (blue beam); blue outlined dots are used to build the reflectivity information representing the corresponding HSI information; blue

319 dashed lines inside the HSI cone represent the two return levels integrated into the

- 320 reflection representation of this HSI cone.
- 321 This procedure accounts for the attenuation correction in the surroundings of dense
- vegetation where sparse vegetation splits the ALS energy into multiple returns (Fig. 5).

For HSI beams with dense first pulse returns caused by the canopy and sparse returns of higher order inside or underneath the vegetation, the top first pulse returns are used to build a continuous surface. Only these top first pulses represent the canopy parts influencing the area integrating the sensor answer of the HSI system.

327 3.2.5 Calculation of the transfer factor X_{cross}

For the transfer of the cross-calibration between the overlapping wavelength domain 328 of 1550 nm (Fig. 4 (7)) and the remaining wavelength, an additional factor ($X_{{\it cross}}$) is 329 introduced into equation (1). X_{cross} is intended to represent differences in illumination 330 between shaded and fully illuminated areas. In fully illuminated areas, $E_{\rm dir}$ and $E_{\rm dif}$ are 331 present. In shaded areas, E_{dir} is absent, and only E_{dif} is present. Thus, X_{cross} adjusts 332 the amount of $E_{\rm dir}$ based on the calibrated and adapted ALS intensity data. Therefore, 333 Equation (1) with the introduced factor X_{cross} is solved by substituting ρ_{HSI} for 1550 334 335 nm with the cross-calibrated ALS reflectance (ρ_{ALS}) (9)

336
$$X_{cross} = \frac{\pi d^2 (L_{HSI} - L_{PHSI})}{E_{dir} * \rho_{ALS} * \tau_{atm}} - \frac{E_{dif}}{E_{dir}}.$$
 (9)

The determined factor X_{cross} (Fig. 6 (7)) is then used to calculate ρ_{HSI} for all remaining wavelengths. This results in corrected HSI reflectance (Fig. 6 (D)).



Fig. 6: Geocoded overview of the input/output data products (A-D) and results of the processing modules (1-7) using non-consecutive numeration corresponding to the detailed workflow diagram (Fig. 4).

343 3.3 Requirements and Assumptions

Considering the following four requirements and assumptions, the presented generic method can be applied to the complete flight campaign, as well as to other system configurations and characteristics. First, one of the main pre-requisites for the crosscalibration is an accurate spectral and geometric co-alignment, which includes the adaptation of the overlapping wavelength domain considering the central wavelength

and bandwidth. Second, it has to be assumed that both sensor systems are 349 geometrically and radiometrically stable during the entire flight campaign. Third, the 350 351 characteristic of the laser pulse regarding amplitude, echo width, and shape of the reflected echo should be known. Thus, the complexity of the underlying object 352 reflection is fully represented, and a radiometric correction is also possible for non-353 horizontal targets [19]. Consequently, the detection of return echoes and the 354 separation into different reflections out of the full-waveform information can be created 355 356 with Gaussian decomposition [25], [19]. Fourth, the approaches for the radiometric calibration of ALS intensities assume that all surface objects diffusively reflect 357 358 according to the Lambertian law. This assumption enables the calculation of diffuse reflectance, which depends on only the object properties, not on the viewing angle. 359

360 4 Results

The introduced radiometric cross-calibration generates an HSI reflectance data cube with reduced shadowing and illumination influences. In the following, these results are presented and evaluated for the test data set, which is strongly influenced by illumination effects. The chapter is divided into a comparison of the adapted intensity information of the overlapping wavelength domain of 1550 nm, an investigation of the corrected HSI data cube, and an evaluation of the potentials for HSI data quality and classification improvements. 368 4.1 Comparison between the overlapping wavelength domain of 1550 nm

A rough visual comparison between the standard reflectance results for HSI (Fig. 7 A) and the reflectance calculated based on the cross-calibration approach (Fig. 7 B) for the wavelength domain of 1550 nm clearly shows the successful correction of illumination influences in the HSI-ALS fused data. Despite the complex illumination situations caused by cloud shadowing, low solar elevation and heterogeneous object exposure, the correction appears consistent thanks to the radiometrically calibrated active ALS signal.



Fig. 7: Overview of one corrected flight line of 1550 nm, with red marked subsets and
profiles used for further accuracy assessment; (A) HSI BOA reflectance of 1550 nm
(no shadow correction); (B) HSI BOA reflectance of 1550 nm (all corrections applied);
(C) Correction factor X_{cross} calculated for the atmospheric transformation to all HSI
wavelengths.

A closer inspection of the reflectance (1550 nm) based on three transects (marked in 382 383 Fig. 7 B with red arrows) confirms the consistency. Transect 1 (Fig. 8) indicates the 384 impact of the cross-calibration to the reflectance values representing the concrete runway in the along-track direction of the flight stripe. Compared to the uncorrected 385 386 reflectance values (red plot), the blue plot alternates at a constant level of approximately 30 % reflectance. The high frequency contrast between the pixels is 387 preserved or enhanced due to a higher signal level, whereas the low frequency 388 389 contrast introduced by illumination differences is compensated for. The same is valid 390 for transect 2 at a lower reflectance level of approximately 8 %, representing the 391 across-track influence intersecting a relatively homogeneous asphalt road. Additional 392 spikes become apparent due to moving cars and retroreflective lane markings not represented equivalently in both sensor responses. Transect 3 extends in the along-393 394 track direction over the complete flight stripe representing its inherent heterogeneity. This transect confirms the results of transects 1 and 2. 395



Fig. 8: Along and across track transects representing reflectance for 1550 nm (red uncorrected, blue corrected), x-axis represent the underlying pixel (1.2 x 1.2 m); (A) along track intersecting the concrete runway; (B) across track intersecting asphalt road; (C) along track intersecting various surface materials.

401 The two scatter plots in Fig. 9 (A) and (B) show the relation between the received ALS 402 power (P_r) (y-axis) and reflectance (x-axis) for the original HSI reflectance (A) and cross-calibrated HSI reflectance (B). The regression lines (in red) and their equation 403 404 (y), as well as the Pearson correlation coefficient (R), are presented. Plot (A) depicts 405 highly uncorrelated information due to the different illumination conditions and differences in the sensor response. However, after the cross-calibration, a close-to-406 407 linear relationship is observed (B). As expected, the spatial distribution of the nonlinear values (under the regression line marked in red Fig. 9 B right) have no correlation with 408 409 solar illumination conditions. The differences between radiometrically uncorrected ALS intensities and cross-calibrated intensities due to varying ALS point density and overall 410 411 surface heterogeneity become apparent. It highlights the indispensability of the 412 radiometric calibration of the ALS data.



414 Fig. 9: Various scatter plots indicating the relationship between ALS data and HSI data 415 in the overlapping wavelength domain of 1550 nm; (A) shows the relation between original HSI data (x-axis) and ALS received power (y-axis); (B) shows the relation 416 417 between the cross-calibrated data (x-axis) and uncorrected ALS received power (y-418 axis); (C) (D) show the influence of different calibration targets ((C) runway, (D) grass) 419 and their overall non-linear relation between original HSI data (x-axes) and cross-420 calibrated data (y-axes). The blue reference lines (x=y) separate the data sets into two 421 parts: black clusters represent pixels that have expectedly higher values after the cross-calibration; red clusters represent pixels that have smaller values after cross-422 calibration; the spatial distributions of the red clusters are shown in the flight stripes on 423 424 the right.

425 Scatter plots (C), (D) represent the relations between the original HSI (x-axes) and the

426 cross-calibrated (y-axes) reflectance for two different calibration targets. Plot (C)

427 results from the calibration on selected pixels from the runway and (D) from grassland.

428 Both plots also show that the relation between ALS and HSI is highly uncorrelated and

429 affected by noise due to the differences of the respective radiation paths and the

430 interaction with the surface objects. Red marked clusters separated by the blue

- 431 reference line (x=y) indicate pixels with unrealistically smaller values after the cross-
- 432 calibration. Their spatial distribution is also shown in the flight lines on the right side. In

addition to complex anisotropic surface behaviour (e.g., solar array, sheet-metal 433 roofing), the smaller values result from a small overestimation of the first HSI 434 reflectance calculation (Fig. 4 (3)) caused by an underestimation of complex diffuse 435 illumination conditions inside small gaps in the clouds. Both plots (Fig. 9 C and D) 436 indicate that the different reflectance characteristics of grassland and concrete due to 437 anisotropy and roughness generate differences in the sensor responses of the two 438 sensors. It is caused by the fact that the calibration targets do not strictly fulfil the 439 440 requirements of a Lambertian surface, and thus both sensor systems still have a 441 surface-dependent characteristic difference in their sensor responses. Also Fig. 7 C representing the correction factor X_{cross} does not only change with direct illumination 442 variation. Different anisotropy and roughness characteristics of the different surfaces 443 444 are still apparent in the factor. Nevertheless, it is assumed that the runway most likely 445 fulfils the Lambertian surface criteria and serves as the final cross-calibration target for 446 all further results. This target sensitivity highlights the relative character of the cross-447 calibration but also emphasizes the opportunity to optimize for different surface characteristics. 448

449 4.2 Corrected HSI data cube

450 The spatial pattern of the derived correction factor (X_{cross}) shown in Fig. 7 C is used to compensate for the unwanted illumination patterns for the remaining wavelength of the 451 452 HSI sensors. The result of this proposed transformation is shown in Fig. 10 B in 453 comparison to the uncorrected HSI reflectance (A). The visual comparison indicates the overall good performance of the method. The patterns of illumination differences 454 that are clearly visible in the HSI reflectance data (A) are eliminated without any 455 456 recognizable artefacts in the transition zones. This fact is also confirmed by the 457 comparison of the selected spectral profiles (Fig. 10, middle). The first spectral 458 comparison of the grassland surface (1) shows that the corresponding spectra are nearly identical before and after the correction. This is due to illumination by direct and 459 diffuse radiation without the influence of shadows. All other example spectra are 460 461 influenced by shadows (red spectra in 2, 3, 4, and 5), exhibiting a clear attenuation. 462 They are located in areas where only diffuse illumination exists, which is not considered 463 in Eq. (9). After the correction, the spectra (blue spectra in 2, 3, 4, and 5) indicate that 464 this lack of direct illumination is compensated for, and the spectra are raised to 465 plausible reflectance values.



Fig. 10: Atmospheric corrected HSI reflectance (back-projected to SWIR sensor
geometry; R = 702 nm, G = 1249 nm, B = 586 nm); (A) without cross-calibration (red
label); (B) cross-calibrated corrected data (blue label); (middle) Comparison of
uncorrected (A) and corrected (B) reflectance spectra for different surface materials (1,
2, 3, 4, 5) influenced by various illumination conditions.



illumination conditions. However, different surface objects are also visible in
homogeneous illuminated areas. This can be explained by small illumination and
viewing differences caused by surface roughness and anisotropic behaviour. Despite
the sensor adaptation, these effects, which influence the sensor responses, are still
inherent in the data.



- Fig. 11: Reflectance difference (Δ=cross-calibrated reflectance original HSI
 reflectance) between adjacent wavelength with their respective colour slices and
 histograms; (A) for 549.3 nm; (B) for 1651.8 nm; locations of reflectance spectra shown
 in Fig. 10 are marked with black crosses.
- 485 4.3 HSI data quality and classification improvements
- 486 A detailed visual comparison of subsets 1 and 2 (red boxes Fig. 7) is presented in Fig.
- 487 12. It is clearly visible that the illumination influence inherent in the original HSI data (A

and D, red border) is corrected (B and E, blue border) without any visual artefacts in 488 489 the transition areas. This circumstance is also confirmed by the difference images (C and F) where the transition between directly illuminated areas and cast shadow areas, 490 491 as well as cloud shadow areas, is very smooth and reasonable. The correction of the solar illumination influence is especially visible at saddle roofs exposed on one side 492 towards the sun, and on the other side, only diffuse radiation is present. In Fig. 12 B, 493 494 these patterns are entirely compensated for. Fig. 12 E indicates that the shadow 495 influencing the canopy representation of the large tree can also be compensated for. All of this indicates the potential of the proposed method, especially for advanced 496 497 vegetation and canopy studies [31], [4], [32], as well as for urban mapping [33], [5].



498

Fig. 12: Detailed comparison of the fusion procedure, and all images are displayed with
1 % linear global stretch; (A) uncorrected HSI reflectance image (RGB) transition zone
between direct illumination and cloud shadow; (B) corrected HSI reflectance image
(RGB) without any illumination artefacts; (C) greyscale difference image (A - B)
indicating areas with less (black) and strong (white) solar illumination influence; same
for (D), (E), (F), except for displaying CIR false colour for (D) and (E).

505 Overall, it is perceptible that the internal contrast inside homogeneous areas, for

506 example, the asphalt road (Fig. 12 B) or the field (Fig. 12 E), is enhanced. However,

507 the difference images (Fig. 12 C and F) indicate relatively homogenous internal

508 patterns for these regions. These enhancements can be explained by contrast 509 stretching due to the elimination of shadow information. Artefacts or structures that are 510 not visible in the original HSI data are not generated. Thus, the cross-calibration 511 enhances the local contrast but does not add inherent ALS speckle to the results. It 512 seems that the spatial sensor adaptation (section 3.2.4) successfully suppresses such 513 artefacts.



514

Fig. 13: Spectral comparison between two adjacent and overlapping flight stripes; (A)
uncorrected HSI reflectance; (B) corrected HSI reflectance; (1, 2, 3, 4) sample spectra
from overlapping pixels (orange and violet = spectra of left flight strip, red and blue =
spectra of right flight strip.

- 520 It results in a seamless mosaic (Fig. 13 B) with a remarkable reflectance match in the
- 521 overlapping pixels (Fig. 13 1, 2, 3, 4). Despite the data acquisition not being

⁵¹⁹ One of the benefits of the cross-calibration is its inherent inter-flight stripe adjustment.

522 perpendicular to the solar principal plane, across-track illumination gradients are not 523 observed (Fig. 13 B and Fig. 8, transect 2). The modifications caused by the cross-524 calibration and their spatial, radiometric and spectral characteristics are also visible in Fig. 14, where the differences between the two overlapping adjacent flight stripes are 525 analysed for two wavelengths (549.3 nm (A, C) and 1651.8 nm (B, D)). The differences 526 527 for the uncorrected reflectance (red border A and B) show strong illumination patterns. However, the differences between the cross-calibrated flight stripes (C, D) do not 528 529 exhibit these patterns. The histograms and statistic assessments indicate a clear 530 tendency towards smaller differences and a more homogeneous distribution. For the 531 relatively short VNIR wavelength of 549.3 nm (A, C), minor reflectance differences caused by illumination are still perceptible due to the stronger diffuse scattering of 532 533 smaller wavelengths. However, the overall tendency towards smaller differences is 534 present. Especially for the SWIR wavelength (B), the illumination patterns are 535 eliminated in the cross-corrected SWIR differences (D). The spatial distribution 536 indicates that only transition areas between surface objects are causing reflectance 537 differences of ±3.7 % standard deviation. The comparison between the adjacent flight stripes indicates that across-track illumination gradients are compensated independent 538 from shadow influence. 539



541 Fig. 14: Reflectance difference (colour slice) between overlapping adjacent flight 542 stripes (grey scale); Δ =left flight stripe(1) - right flight stripe(2); histograms indicate the 543 distribution of the resulting differences; (A, B) difference between uncorrected HSI 544 reflectance (red border) for overlapping (A) 549.3-nm and (B) 1651.8-nm bands; (C, 545 D) difference between cross-calibrated HSI reflectance (blue border) for overlapping 546 (C) 549.3-nm and (D) 1651.8-nm bands.



Fig. 15 Subsets (in sensor coordinates) of supervised Support vector machine
classification results (7 classes, 3 iterations) and their corresponding confusion matrix;
(A) based on reflectance without cross-calibration; (B) based on cross-calibrated
reflectance.

552 To assess the benefits for application and classification purposes, a supervised

553 support vector machine (SVM) classification [34] has been carried out for the original

HSI data (Fig. 15 A) and the cross-calibrated data (B) (Fig. 15). For the cross-calibrated

data, the classification results in an overall accuracy of 98.56 % and a kappa coefficient

of 0.98. This contrasts with the overall accuracy of 78.79 % and kappa coefficient of

0.71 for the original HSI data. The corrected data clearly shows a classification 557 improvement. Based on the confusion matrix (Fig. 15 A), it can be shown that for the 558 original HSI data, concrete pixels are often falsely classified as asphalt and vice versa. 559 Additionally, grass surfaces are often misclassified as trees and vice versa. Also 560 remarkable are the tin roofs, which are often falsely classified as asphalt. These 561 misclassifications can be explained by a higher spectral similarity between these 562 classes, especially under shadowed conditions. After the correction (Fig. 15 B 563 564 confusion matrix), misclassifications are significantly reduced, and the classifications of concrete, asphalt, trees, grass and tin roofs especially profit from the corrections. 565 566 Additional tests with a spectral angle mapper (SAM) classification, usually more robust to variations of albedo, performed poorer for the corrected data then SVM classification 567 performed for the uncorrected data. The overall poorer SAM classification results for 568 569 the uncorrected data also indicate nearly identical problems with the separation of trees 570 and grass as well as with the separation of soil, asphalt and concrete. These 571 classification results imply that the cross-calibrated reflectance clusters representing 572 certain surface objects are more separated and have smaller cluster variability. These 573 are promising results for any type of more specialized application dealing with vegetation or urban classifications, where the influence of shadows always hampers 574 575 the results.

576 **5 Discussion**

577 The results of the proposed illumination correction of the HSI data based on the cross-578 calibration with the ALS intensity data seem promising for all urban and vegetation 579 settings influenced by cast shadows. Additionally, extreme complex illumination 580 conditions, such as cloud or terrain shadowing, can be improved. A significant 581 enhancement is indicated compared to the exclusive use of HSI data. The cross-

582 calibration is only a relative calibration; nevertheless, the combination has the potential 583 to eliminate typically disturbing effects in passive sensor data. The benefits of 584 compensating for illumination differences are evident when considering de-shadowing, 585 across-track illumination correction, albedo levelling, and mosaicking. With the active 586 support, illumination changes over time beside shadow influences are compensated. 587 This is especially beneficial for the interpretation and classification of data acquired 588 during long-lasting flight campaigns.

589 However, some requirements and assumptions considering the sensor systems, 590 characteristics and flight parameters have to be fulfilled to generate such results. The 591 ray tracing-based approach is necessary to compensate for the influence of the different sensor responses, especially concerning tree canopies. Additional work must 592 593 be performed to fulfil the requirements for an operational application in HSI data pre-594 processing. The overall radiative interaction between the sensors and various surface 595 objects considering anisotropic behaviour and roughness differences must be 596 addressed. In addition, the sensor adaptation by filtering the point cloud should be 597 evaluated in detail. Additionally, the influence of the enhanced HSI data on more specific classification applications should be addressed in the future. The proposed 598 method can be helpful, especially for the exploration of the different sensor responses. 599 600 Due to the physically based adaptation, the method is generic and can be adopted to 601 different ALS wavelength. All of these efforts will profit from upcoming multiplewavelength ALS systems and thereby bring airborne imaging spectroscopy closer to 602 603 real reflectance measurement.

604 Conclusion

605 Three key findings can be drawn from the in-flight cross-calibration of ALS and HSI 606 sensors:

In general, de-shadowing, illumination correction, albedo levelling and
 mosaicking during HSI pre-processing can be enhanced by using ALS intensity
 information.

As a consequence, classification can be improved by the fusion of intensity data
from ALS and HSI. For example, the classification of heterogeneous urban and
vegetated surfaces, which are spectrally confirmed under shadowed conditions,
benefit from the data fusion.

614 3. A point-cloud based combination and adaptation of both sensor responses on
615 a raw data level is necessary, to properly characterize the morphological
616 heterogeneity of vegetated and urban surfaces.

617 The proposed method is the first in-flight airborne HSI and ALS intensity data fusion. It is based on a rigorous radiometric correction of the ALS intensity data and cross-618 619 calibration with the HIS data. The physically based correction results in realistic HSI 620 reflectance values where relief, illumination, shadows and directional effects have 621 been compensated and corrected for. The method provides a suitable basis to explore 622 and adapt the sensor responses and develop unexploited synergies concerning the 623 radiometric enhancement of both sensors. The results show that a combination of 624 active ALS and passive HSI systems can strengthen the overall data quality and classification accuracy of HSI reflectance, especially for heterogeneous vegetation 625 626 structures and all urban settings. The data fusion is useful for complex illumination and 627 shadowing situations, for example, clouds and rough terrain. The presented 628 methodology and promising results can be applied for various specialized applications, 629 such as tree-species identification and high-spatial resolution urban mapping, which 630 rely on constant and comparable illumination conditions. Our results give evidence 631 that, beyond the ALS accurate range measurement, these systems can support and

enhance HSI pre-processing with intensity information, especially for heterogeneous
urban and vegetation surface coverage. The combination of both sensors achieves a
true reflectance measurement that accounts for shadowing, directional effects and
atmospheric heterogeneities. With future advances, such as multispectral ALS
systems, a rigorous data fusion approach will be essential to extract high-resolution
information and increase the quality of mapping applications.

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645 **References**

- M. Dalponte, L. Bruzzone, and D. Gianelle, 'Fusion of Hyperspectral and LIDAR Remote
 Sensing Data for Classification of Complex Forest Areas', *IEEE Trans. Geosci. Remote Sens.*, vol. 46, no. 5, pp. 1416–1427, 2008.
- 649 [2] G. P. Asner *et al.*, 'Carnegie Airborne Observatory-2: Increasing science data
 650 dimensionality via high-fidelity multi-sensor fusion', *Remote Sens. Environ.*, vol. 124, pp.
 651 454–465, Sep. 2012.
- [3] H. Buddenbaum, S. Seeling, and J. Hill, 'Fusion of full-waveform lidar and imaging
 spectroscopy remote sensing data for the characterization of forest stands', *Int. J. Remote Sens.*, vol. 34, no. 13, pp. 4511–4524, 2013.
- M. Alonzo, B. Bookhagen, and D. A. Roberts, 'Urban tree species mapping using
 hyperspectral and lidar data fusion', *Remote Sens. Environ.*, vol. 148, pp. 70–83, May
 2014.
- U. Heiden, W. Heldens, S. Roessner, K. Segl, T. Esch, and A. Mueller, 'Urban structure
 type characterization using hyperspectral remote sensing and height information', *Landsc. Urban Plan.*, vol. 105, no. 4, pp. 361–375, Apr. 2012.
- [6] Yanfeng Gu, Qingwang Wang, Xiuping Jia, and J. A. Benediktsson, 'A Novel MKL Model
 of Integrating LiDAR Data and MSI for Urban Area Classification', *IEEE Trans. Geosci. Remote Sens.*, vol. 53, no. 10, pp. 5312–5326, Oct. 2015.
- 664 [7] G. P. Asner *et al.*, 'Carnegie airborne observatory: in-flight fusion of hyperspectral 665 imaging and waveform light detection and ranging for three-dimensional studies of 666 ecosystems', *J. Appl. Remote Sens.*, vol. 1, no. 1, pp. 013536–013536, 2007.

- [8] T. U. Kampe, 'NEON: the first continental-scale ecological observatory with airborne
 remote sensing of vegetation canopy biochemistry and structure', *J. Appl. Remote Sens.*,
 vol. 4, no. 1, p. 043510, Mar. 2010.
- M. Brell, C. Rogass, K. Segl, B. Bookhagen, and L. Guanter, 'Improving Sensor Fusion:
 A Parametric Method for the Geometric Coalignment of Airborne Hyperspectral and Lidar
 Data', *IEEE Trans. Geosci. Remote Sens.*, vol. 54, no. 6, pp. 3460–3474, 2016.
- [10] H. Torabzadeh, F. Morsdorf, and M. E. Schaepman, 'Fusion of imaging spectroscopy and
 airborne laser scanning data for characterization of forest ecosystems A review', *ISPRS J. Photogramm. Remote Sens.*, vol. 97, pp. 25–35, Nov. 2014.
- [11] Q. Zhang, V. P. Pauca, R. J. Plemmons, and D. D. Nikic, 'Detecting objects under shadows by fusion of hyperspectral and lidar data: A physical model approach', in *Proc.*5th Workshop Hyperspectral Image Signal Process.: Evol. Remote Sens, 2013, pp. 1–4.
- 679 [12] E. J. lentilucci, 'Leveraging lidar data to aid in hyperspectral image target detection in the 680 radiance domain', 2012, pp. 839007-839007–12.
- [13] A. Roncat, C. Briese, and N. Pfeifer, 'A Comparison of LIDAR Reflectance and Radiometrically Calibrated Hyperspectral Imagery', *ISPRS - Int. Arch. Photogramm. Remote Sens. Spat. Inf. Sci.*, pp. 705–710, Jun. 2016.
- [14] P. J. Hartzell *et al.*, 'Comparison of synthetic images generated from LiDAR intensity and
 passive hyperspectral imagery', in *2014 IEEE Geoscience and Remote Sensing Symposium*, 2014, pp. 1345–1348.
- [15] S. Hagstrom and J. Broadwater, 'Generating passive NIR images from active LIDAR',
 2016, p. 98320G.
- [16] J. U. H. Eitel *et al.*, 'Beyond 3-D: The new spectrum of lidar applications for earth and ecological sciences', *Remote Sens. Environ.*, vol. 186, pp. 372–392, Dec. 2016.
- [17] D. Schläpfer, R. Richter, and A. Damm, 'Correction of shadowing in imaging spectroscopy
 data by quantification of the proportion of diffuse illumination', 8th SIG- EARSeL Imaging
 Spectrosc. Workshop Nantes, p. 10, 2013.
- [18] C. Briese, M. Pfennigbauer, H. Lehner, A. Ullrich, W. Wagner, and N. Pfeifer,
 'Radiometric calibration of multi-wavelength airborne laser scanning data', *ISPRS Ann Photogramm Remote Sens. Spat Inf Sci*, vol. 1, no. 7, pp. 335–340, 2012.
- [19] W. Wagner, 'Radiometric calibration of small-footprint full-waveform airborne laser
 scanner measurements: Basic physical concepts', *ISPRS J. Photogramm. Remote Sens.*, vol. 65, no. 6, pp. 505–513, Nov. 2010.
- F. Coren and P. Sterzai, 'Radiometric correction in laser scanning', *Int. J. Remote Sens.*,
 vol. 27, no. 15, pp. 3097–3104, Aug. 2006.
- [21] A. Kashani, M. Olsen, C. Parrish, and N. Wilson, 'A Review of LIDAR Radiometric
 Processing: From Ad Hoc Intensity Correction to Rigorous Radiometric Calibration',
 Sensors, vol. 15, no. 11, pp. 28099–28128, Nov. 2015.
- 705 [22] 'HySpex, Norsk Elektro Optikk'. [Online]. Available: http://www.hyspex.no/index.php.
 706 [Accessed: 19-May-2015].
- [23] K. Lenhard, A. Baumgartner, and T. Schwarzmaier, 'Independent Laboratory
 Characterization of NEO HySpex Imaging Spectrometers VNIR-1600 and SWIR-320me', *IEEE Trans. Geosci. Remote Sens.*, vol. 53, no. 4, pp. 1828–1841, Apr. 2015.
- 710 [24] 'RIEGL RIEGL Laser Measurement Systems'. [Online]. Available: http://www.riegl.com/.
 711 [Accessed: 19-May-2015].
- [25] W. Wagner, A. Ullrich, V. Ducic, T. Melzer, and N. Studnicka, 'Gaussian decomposition and calibration of a novel small-footprint full-waveform digitising airborne laser scanner', *ISPRS J. Photogramm. Remote Sens.*, vol. 60, no. 2, pp. 100–112, Apr. 2006.
- [26] L. Guanter, K. Segl, B. Sang, L. Alonso, H. Kaufmann, and J. Moreno, 'Scene-based spectral calibration assessment of high spectral resolution imaging spectrometers', *Opt. Express*, vol. 17, no. 14, p. 11594, Jul. 2009.
- [27] R. Richter, T. Kellenberger, and H. Kaufmann, 'Comparison of Topographic Correction Methods', *Remote Sens.*, vol. 1, no. 3, pp. 184–196, Jul. 2009.
- [28] L. Guanter, K. Segl, and H. Kaufmann, 'Simulation of Optical Remote-Sensing Scenes
 With Application to the EnMAP Hyperspectral Mission', *IEEE Trans. Geosci. Remote Sens.*, vol. 47, no. 7, pp. 2340–2351, Jul. 2009.

- [29] L. Guanter, K. Segl, and H. Kaufmann, 'Simulation of Optical Remote-Sensing Scenes
 With Application to the EnMAP Hyperspectral Mission', *IEEE Trans. Geosci. Remote Sens.*, vol. 47, no. 7, pp. 2340–2351, Jul. 2009.
- [30] A. Berk *et al.*, 'MODTRAN cloud and multiple scattering upgrades with application to AVIRIS', *Remote Sens. Environ.*, vol. 65, no. 3, pp. 367–375, 1998.
- [31] M. Alonzo, B. Bookhagen, J. P. McFadden, A. Sun, and D. A. Roberts, 'Mapping urban forest leaf area index with airborne lidar using penetration metrics and allometry', *Remote Sens. Environ.*, vol. 162, pp. 141–153, Jun. 2015.
- [32] A. Clasen *et al.*, 'Spectral Unmixing of Forest Crown Components at Close Range,
 Airborne and Simulated Sentinel-2 and EnMAP Spectral Imaging Scale', *Remote Sens.*,
 vol. 7, no. 11, pp. 15361–15387, Nov. 2015.
- [33] S. Roessner, K. Segl, U. Heiden, and H. Kaufmann, 'Automated differentiation of urban surfaces based on airborne hyperspectral imagery', *IEEE Trans. Geosci. Remote Sens.*, vol. 39, no. 7, pp. 1525–1532, Jul. 2001.
- [34] C.-C. Chang and C.-J. Lin, 'LIBSVM: a library for support vector machines', *ACM Trans. Intell. Syst. Technol. TIST*, vol. 2, no. 3, p. 27, 2011.