

3D NLCG inversion algorithm for CSEM data - discussion about mesh design -

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Introduction

We want to discuss the mesh design for 3D non-linear conjugate gradient (NLCG) inversion of controlled-source electromagnetic (CSEM) data using our 3D finite-element modelling code [1] implemented in the inversion software *emilia* [2, 3].

Gradient Computation

For the NLCG algorithm, gradients of the objective function Φ wrt. the model parameters m_k have to be calculated. The gradient of the data functional $\frac{\partial \Phi_d}{\partial m_k}$ is the crucial part in this computation obtained after [4] as

$$\frac{\partial \Phi_d}{\partial m_k} = -2Re \left[- \sum_{n=1}^N (\Delta Z_n)^* \gamma_n^T A^{-1} \left(\frac{\partial A}{\partial m_k} E_1 \right) - \sum_{n=1}^N (\Delta Z_n)^* \gamma_n^T A^{-1} \left(\frac{\partial A}{\partial m_k} E_2 \right) \right], \quad (1)$$

where $\Delta Z_n = [(d_n^{obs} - F_n(\mathbf{m})) / \epsilon_n^2]$, n is the number of data, A the system matrix of the forward problem and E_1 and E_2 the forward solutions of two source polarisations. The factor γ comprises the interpolator functions of the finite-element method and linear combinations of several electric and magnetic fields.

Regularisation

For the model regularisation term, we have to calculate the inverse model covariance matrix $C_m^{-1} = C^T C$ (C : smoothness matrix), which we construct with a first order difference operator as suggested in [5] for tetrahedral elements. Taking the neighbouring element relations into account, we know, that two neighbouring elements i, j share a face f , while only inner faces and only Earth cells are considered, so that

$$C_{f,i} = -1 \quad \text{and} \quad C_{f,j} = 1. \quad (2)$$

References

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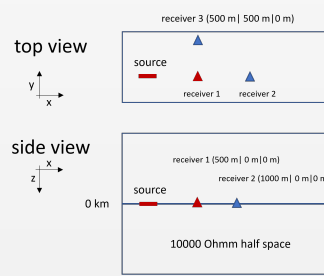
1. Mesh Design

The general **correctness of the gradient computations** can be verified by comparing $\frac{\partial \Phi_d}{\partial m_k}$ (setting $\Delta Z_n = 1.0$) with sensitivities obtained with the perturbation method (Table 1) using one active receiver.

Table 1: Comparison of element gradients obtained with eq. 1 with element sensitivities obtained using the perturbation method (model parameter perturbation $dm = 0.01$) of a mesh refined only in the central region (Fig. 1). For larger elements (e.g. element 4), the perturbation method is quite sensitive to the choice of dm , which shows, that the method only works for a gross verification of the gradient values.

element	$\frac{\partial \Phi_d}{\partial m_k}$ for Z_{xy}	perturbation for Z_{xy}	$\frac{\partial \Phi_d}{\partial m_k}$ for Z_{yx}	perturbation for Z_{yx}
1 (receiver 1)	21.1	20.9	-7.2	-6.3
2 (receiver 2)	13.5	13.5	-4.3	-4.3
3 (receiver 3)	9.4	9.4	-6.9	-6.9
4 (250 m 0 m 300 m)	-6.7	-7.5	1.7	1.5

a) model



b) gradients

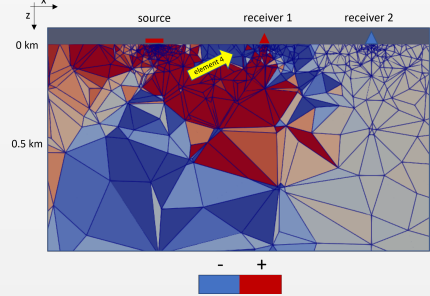


Figure 1: Slices through a 3D model (a) and the corresponding finite-element mesh with coloured gradients for the Z_{xy} data component of receiver 1 refined only in the central region around the source and receivers (b).

How to design the tetrahedral meshes, so that the gradient computations are accurate enough?

- Receiver elements need to be **small** to obtain accurate forward responses at the receivers.
- Do we have to design **more regular meshes** for gradient computation?
- How dense should a mesh be between receiver sites for expedient gradient computation?
- Is it meaningful to use **different meshes for forward computation and inversion (dual-mesh approach)**, although the forward solution vectors and system matrices (cf. eq. 1) can be re-used for gradient computation?

2. Refinement

Is automatic mesh refinement at every inversion step expedient for 3D inversion?

- only practicable, when using a dual-mesh approach
- idea: run the inversion on a coarse mesh without refinement, refine the best-fitting model, this refined model serves as the start model for a second inversion (cf. Fig. 2).

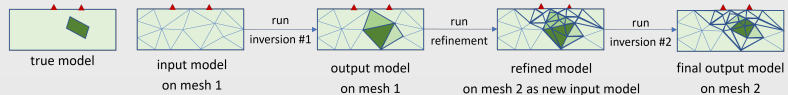


Figure 2: Sketch of a mesh refinement strategy for inversion.

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